

IT NO. UMTA-MA-06-0074-81-1

HE
18.5
.A37
no.
DOT-
TSC-
UMTA-
80-44

PASSENGER FLOW ANALYSIS, 1978, RIVERSIDE LINE, MBTA

Betty S. Kwok

U.S. DEPARTMENT OF TRANSPORTATION
RESEARCH AND SPECIAL PROGRAMS ADMINISTRATION
Transportation Systems Center
Kendall Square
Cambridge MA 02142



1726708
AUGUST 1981
FINAL REPORT



DOCUMENT IS AVAILABLE TO THE PUBLIC
THROUGH THE NATIONAL TECHNICAL
INFORMATION SERVICE, SPRINGFIELD,
VIRGINIA 22161

Prepared for

U.S. DEPARTMENT OF TRANSPORTATION
URBAN MASS TRANSPORTATION ADMINISTRATION
Office of Planning Management and Demonstrations
Office of Transportation Management
Washington DC 20590

NOTICE

This document is disseminated under the sponsorship of the Department of Transportation in the interest of information exchange. The United States Government assumes no liability for its contents or use thereof.

NOTICE

The United States Government does not endorse products or manufacturers. Trade or manufacturers' names appear herein solely because they are considered essential to the object of this report.

HE
18.5
AB7
no.
DOT-TSC-UMTA
R0-44

Technical Report Documentation Page

| | | | |
|---|--|--|-----------|
| 1. Report No. UMTA-MA-06-0074-81-1 | 2. Government Accession No. | 3. Recipient's Catalog No. • | |
| 4. Title and Subtitle PASSENGER FLOW ANALYSIS, 1978 RIVERSIDE LINE, MBTA | | 5. Report Date August 1981 | |
| 7. Author(s) Betty S. Kwok | | 6. Performing Organization Code DTS-231 | |
| 9. Performing Organization Name and Address U.S. Department of Transportation Research and Special Programs Administration Transportation Systems Center Cambridge MA 02142 | | 8. Performing Organization Report No. DOT-TSC-UMTA-80-44 | |
| 12. Sponsoring Agency Name and Address U.S. Department of Transportation Urban Mass Transportation Administration Office of Planning Management and Demonstration Office of Transportation Management Washington DC 20590 | | 10. Work Unit No. (TRAIS) UM037/R0721 | |
| 15. Supplementary Notes | | 11. Contract or Grant No. | |
| 16. Abstract | | 13. Type of Report and Period Covered Final Report 1977-1979 | |
| In order to complete a set of passenger flow estimates for use in a simulation model of a light rail line, a count of passenger movement was made at randomly selected stations in the underground section. Above-ground stations had been studied a year earlier. Eight surveyors were employed during one Monday through Friday period. The model which makes the data tractable is an analysis of variance model, with logarithmic transforms of the data. Although a satisfactory fit was obtained, discrepancies between the treatment of the 1977 and 1978 results made a validation necessary before the methods could be recommended for general use. | | 14. Sponsoring Agency Code UPM-40 | |
| For planning purposes, information about the volume of ridership is essential. This study has shown that sufficiently accurate estimates can be gained without expending huge amounts of labor and money. | | <p>DEPARTMENT OF TRANSPORTATION</p> <p>JUL 9 1982</p> | |
| 17. Key Words Passenger Counts, Transit Demand ANOVA, Light Rail Line, MBTA, Statistical Analysis | 18. Distribution Statement DOCUMENT IS AVAILABLE TO THE PUBLIC THROUGH THE NATIONAL TECHNICAL INFORMATION SERVICE, SPRINGFIELD, VIRGINIA 22161 | | |
| 19. Security Classif. (of this report) Unclassified | 20. Security Classif. (of this page) Unclassified | 21. No. of Pages 104 | 22. Price |



PREFACE

The sample design and passenger flow estimation work described in this study was performed under Project Plan Agreement UM-937, sponsored by the Urban Mass Transportation Administration, Office of Planning Management and Demonstrations, Office of Transportation Management. The work was undertaken to develop a methodology of estimating the distribution of passenger flow for the Light Rail Transit at the underground stations. The techniques are developed in the context of the Massachusetts Bay Transit Authority - Riverside Line, but could be expanded to accommodate other transit properties with appropriate modifications. TSC Technical Program Manager is Mary Roos, DTS-722.

METRIC CONVERSION FACTORS

Approximate Conversions to Metric Measure

| Symbol | When You Know | Multiply by | To Find | Symbol | When You Know | Multiply by | To Find | | |
|---------------------------|---------------|--------------------|--------------------|---------------|---------------|---------------|---------|--|--|
| <u>LENGTH</u> | | | | | | | | | |
| inches | 2.5 | centimeters | millimeters | inches | 0.04 | inches | | | |
| feet | 30 | centimeters | centimeters | inches | 0.4 | feet | | | |
| yards | 0.9 | meters | meters | feet | 3.3 | feet | | | |
| miles | 1.4 | kilometers | kilometers | yards | 1.1 | yards | | | |
| <u>AREA</u> | | | | | | | | | |
| square inches | 6.5 | square centimeters | square centimeters | square inches | 0.16 | square inches | | | |
| square feet | 0.09 | square meters | square meters | square feet | 1.2 | square feet | | | |
| square yards | 0 | square meter | square meter | square yards | 0.4 | square yards | | | |
| square miles | 2.6 | square kilometers | hectares | square miles | 2.6 | hectares | | | |
| acres | 0.4 | hectares | hectares | | | | | | |
| <u>MASS (weight)</u> | | | | | | | | | |
| ounces | 20 | grams | grams | ounces | 0.03 | ounces | | | |
| pounds | 0.45 | kilograms | kilograms | pounds | 2.2 | pounds | | | |
| short tons | 0.9 | tonnes | tonnes | short tons | 1.1 | short tons | | | |
| (2000 lb) | | | | | | | | | |
| <u>VOLUME</u> | | | | | | | | | |
| teaspoons | 6 | milliliters | milliliters | teaspoons | 0.03 | fluid ounces | | | |
| tablespoons | 18 | milliliters | milliliters | tablespoons | 2.1 | ounces | | | |
| fluid ounces | 30 | liters | liters | fluid ounces | 1.06 | liters | | | |
| cups | 0.24 | liters | liters | cups | 0.26 | gallons | | | |
| pints | 0.47 | liters | liters | pints | 3.6 | cubic feet | | | |
| quarts | 0.95 | liters | liters | quarts | 1.3 | cubic yards | | | |
| gallons | 3.8 | cubic meters | cubic meters | gallons | | | | | |
| cubic feet | 0.03 | cubic meters | cubic meters | | | | | | |
| cubic yards | 0.76 | cubic meters | cubic meters | | | | | | |
| <u>TEMPERATURE (FAH.)</u> | | | | | | | | | |
| Fahrenheit | 5-9 | Celsius | Celsius | Temperature | 0/5 (from 32) | Temperature | | | |
| temperature | subtracting | temperature | temperature | Temperature | 32 | 36 | | | |
| | 321 | | | 0 | 40 | 60 | | | |
| | | | | 20 | 40 | 60 | | | |
| | | | | 32 | 40 | 60 | | | |
| | | | | 50 | 60 | 80 | | | |
| | | | | 68 | 80 | 100 | | | |
| | | | | 86 | 100 | 120 | | | |
| | | | | 104 | 120 | 140 | | | |
| | | | | 122 | 140 | 160 | | | |

TABLE OF CONTENTS

| <u>Section</u> | <u>Page</u> |
|---|-------------|
| I. INTRODUCTION..... | 1 |
| II. THE SURVEY PLAN..... | 2 |
| III. DATA EDITING..... | 8 |
| IV. SURVEY DATA ANALYSIS..... | 12 |
| V. STATISTICAL MODEL TO PREDICT DATA GAPS..... | 25 |
| VI. EVALUATION OF SURVEY RESULTS..... | 48 |
| VII. CONCLUSION..... | 51 |
| APPENDIX 1 - SURVEYOR DATA..... | 1-1 |
| APPENDIX 2 - MBTA FILE STRUCTURE..... | 2-1 |
| APPENDIX 3 - PROGRAM EXTRAC..... | 3-1 |
| APPENDIX 4 - PROGRAMS EDIT AND EDIT1..... | 4-1 |
| APPENDIX 5 - PROGRAMS EDIT2 AND EDIT3..... | 5-1 |
| APPENDIX 6 - PROGRAM SEPAR..... | 6-1 |
| APPENDIX 7 - FINAL OUTPUTS: PAKRIV AND PAKLEC.. | 7-1 |
| APPENDIX 8 - PROGRAM PROPFL..... | 8-1 |
| APPENDIX 9 - STATION PROFILE: PAKPFL..... | 9-1 |
| APPENDIX 10 - PROGRAM CONTRAC..... | 10-1 |
| APPENDIX 11 - PROGRAM COMBIN..... | 11-1 |
| APPENDIX 12 - PROGRAM ESTRAG..... | 12-1 |
| APPENDIX 13 - ANOVA RESULTS..... | 13-1 |

LIST OF ILLUSTRATIONS

| <u>Figure</u> | | <u>Page</u> |
|---|----|-------------|
| 1. SCHEDULING OF THE PASSENGER SURVEY..... | 5 | |
| 2. DISTRIBUTION OF LOADING PASSENGERS: CASE 1..... | 17 | |
| 3. DISTRIBUTION OF UNLOADING PASSENGERS: CASE 1..... | 18 | |
| 4. DISTRIBUTION OF LOADING PASSENGERS: CASE 2..... | 20 | |
| 5. DISTRIBUTION OF UNLOADING PASSENGERS: CASE 2..... | 21 | |
| 6. DISTRIBUTION OF LOADING PASSENGERS: CASE 3..... | 23 | |
| 7. DISTRIBUTION OF UNLOADING PASSENGERS: CASE 3..... | 24 | |
| 8. PLOT OF THE RESIDUALS, E_{IJ} , VS. THE PREDICTED VALUE, \hat{R}_{IJ} | 34 | |
| 9. NORMALITY PLOT OF THE STANDARDIZED RESIDUALS (UNTRANSFORMED DATA)..... | 36 | |
| 10. PLOT OF PREDICTED VALUES, \hat{R}_{IJ} , VS. THE ACTUAL, R_{IJ} (UNTRANSFORMED DATA)..... | 37 | |
| 11. PLOT OF THE RESIDUALS, E_{IJ} , VS. THE PREDICTED VALUES, \hat{R}_{IJ} (TRANSFORMED DATA)..... | 45 | |
| 12. NORMALITY PLOT OF THE STANDARDIZED RESIDUALS, E_{IJ} (TRANSFORMED DATA)..... | 46 | |
| 13. PLOT OF THE PREDICTED VALUES, \hat{R}_{IJ} , VS. THE ACTUAL, R_{IJ} | 47 | |
| 14. PROFILE OF LOADING PASSENGERS AT PARK STREET STATION, 1978 (TO RIVERSIDE)..... | 52 | |

LIST OF TABLES

| <u>Table</u> | <u>Page</u> |
|---|-------------|
| 1. SURVEY PLAN..... | 7 |
| 2. MBTA FILE STRUCTURE..... | 9 |
| 3. EDITING PROGRAMS..... | 10 |
| 4. OBSERVED PASSENGER LOADING RATES AT STATIONS (TRAINS TO RIVERSIDE)..... | 13 |
| 5. OBSERVED PASSENGER UNLOADING RATES AT STATIONS (TRAINS TO RIVERSIDE)..... | 13 |
| 6. OBSERVED PASSENGER LOADING RATES AT STATIONS (TRAINS TO NORTH STATION)..... | 14 |
| 7. OBSERVED PASSENGER UNLOADING RATES AT STATIONS (TRAINS TO NORTH STATION)..... | 14 |
| 8. ANOVA RESULTS ON RIVON.MTY: MODEL (2) ANALYSIS OF VARIANCE FOR THE REGRESSION (UNTRANSFORMED DATA). | 32 |
| 9. ANOVA RESULTS ON RIVON.MTY: MODEL (3) ANALYSIS OF VARIANCE FOR THE REGRESSION (TRANSFORMED DATA) | 39 |
| 10. ESTIMATED LOADING RATE (ALL RIVERSIDE TRAINS).... | 49 |
| 11. ESTIMATED UNLOADING RATES (ALL RIVERSIDE TRAINS) | 49 |
| 12. ESTIMATED LOADING RATES (ALL NORTH STATION TRAINS)..... | 50 |
| 13. ESTIMATED UNLOADING RATES (ALL NORTH STATION TRAINS)..... | 50 |

I. Introduction

This paper presents a sampling scheme and an estimation methodology to approximate passenger flows at a system of underground stations. The resulting data will be calibrated into a simulation model whose objective is to optimize the scheduling of the Light Rail Vehicle (LRV) to meet the daily changing passenger demands. Such an effort is part of an operation analysis system designed by the Transit Systems Branch, Urban Systems Division, Office of Ground Systems, to assist transit properties in their management of transit systems maintenance and operations.

When the LRV's were introduced in January of 1977 to Boston's Massachusetts Bay Transit Authority (MBTA) to gradually replace the old PCC's (President Conference Committee) on the Green Line, it was deemed necessary by the U.S. Department of Transportation, who funded 80% of the Boeing made cars, to identify areas of operational improvement and to conduct cost reduction studies. The project, sponsored by the Department's Urban Mass Transportation Administration, aims at employing simple analytical and data management tools to efficiently develop a prototype operations analysis system which can be modified and applied to various transit properties to fit their specific transit management needs.

Specifically, using MBTA's Riverside Line as the experimental unit, this study collects and analyzes passenger data at the thirteen underground stations. Thirteen daily profiles

of passenger loading and unloading rates are estimated so that the distribution of passenger flow at any given station at any time can be obtained. By varying the headways (and thus the schedules) of the trains, one can arrive at the optimal train schedule to accommodate the expected passenger demand.

II. The Survey Plan

A. Knowledge gained from the Survey at the Surface Stations

In May 1977, a sample of LRV trips to and from Riverside was selected and the loading and unloading passenger counts were taken by an onboard surveyor. This was done only for that part of the trip when the train remained on the surface and when the patrons of the LRV were allowed to board and alight through only one door. The underground stations pose a more complex problem. The amount of patronage increases several folds; all the trains are merged onto one track; and at least three doors are open as a train pulls in the station. A more efficient counting procedure is necessary, so that the distribution of passenger flow at these stations for the Riverside trains can be estimated with some degree of confidence without the investment of a large amount of resource and time.

Results of the analysis of 1977 surface station data have proved useful not only in the delineation of the sampling plan for the underground stations, but also in the verification of the resulted passenger profile thus obtained. First, one major finding in the analysis indicates an insignificant day to day difference in the total passenger volume using the LRV.

Second, it was also confirmed by statistical chi-square tests that each surface station holds in general a constant market share of the total passenger volume both for the morning and the afternoon hours. Hence it was possible, given a total trip passenger volume at any time, to ascertain an expected passenger volume from a certain station on the way. It is safe to deduce, therefore, that "station" (or location) and "time of day" are the two most important variables which determine potential passenger flows onto the LRV's. That is, we propose to investigate how the rate of passenger flow varies systematically with the two factors. The length of the headway, another essential parameter, will of course determine the actual congestion and the waiting time.

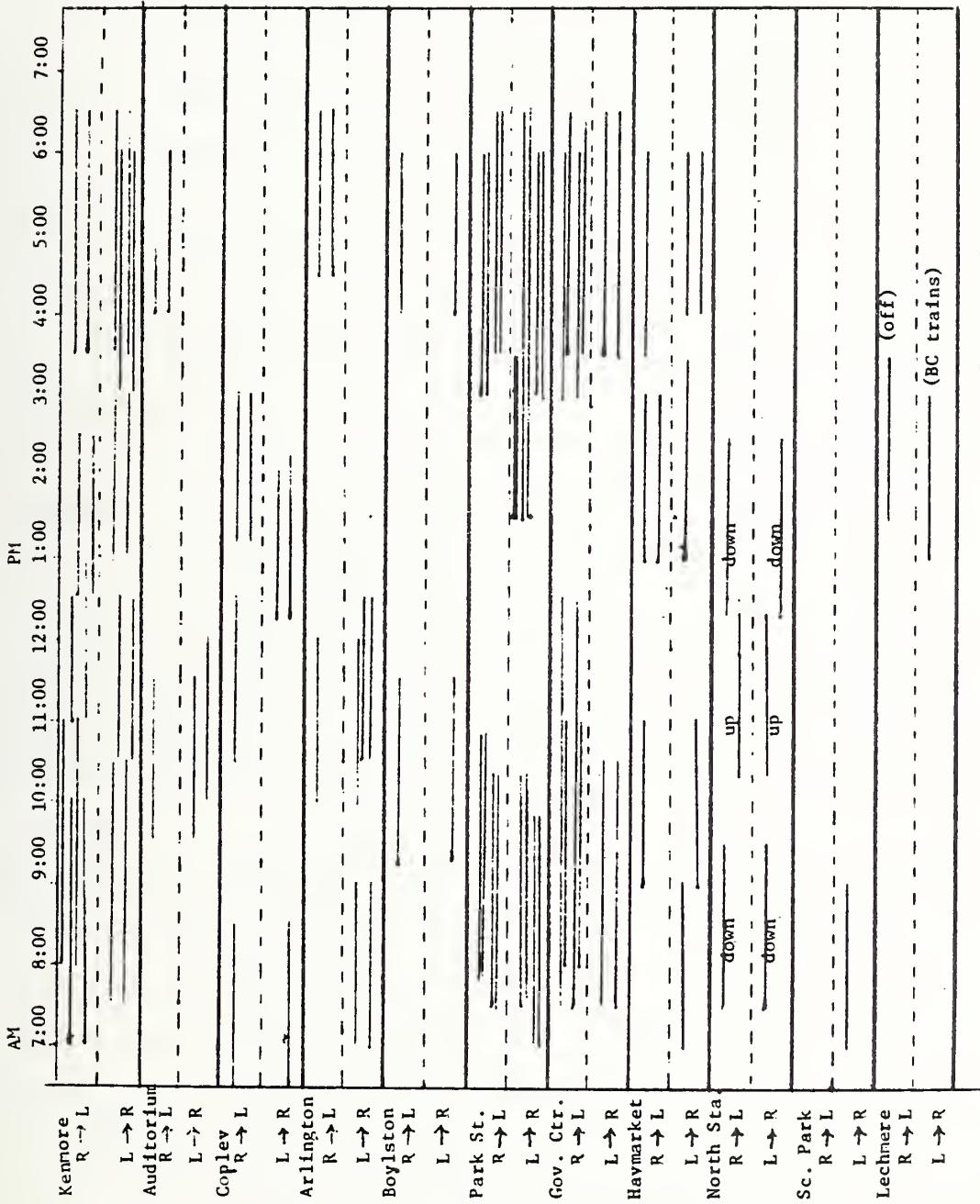
B. The Survey Plan at the Underground Stations

In May 1978, a new survey plan was devised whereby H. H. Aerospace, Inc., a minority contractor, would send a team of eight surveyors to the thirteen underground stations. Their mission: to collect passenger data on the Riverside trains, both inbound and outbound.

It is necessary to discuss the survey plan and field assignment in some detail because it is precisely the design of the survey that enables the analyst to draw meaningful inference from the survey data. The objective of the survey is to derive a representative daily distribution of passenger flows either by summarizing the survey data or by means of estimation using a simple statistical model. The use of a

statistical model economizes the number of observations required, because variation in the data is minimized by the control variables in the model. For example, indicator variables such as the location of the station and the time of the day probably explain much of the data variance, and a two factor analysis of variance (ANOVA) model seems most appropriate. The implementation of the model is the major criterion for the survey design.

Two other constraints are the time span (five days) in which the survey is to be conducted, and the labor resource (eight surveyors). The number of surveyors assigned to a station depends on the amount of passenger traffic the station receives. For example, four surveyors are assigned to Park Street Station at peak hours, while Auditorium or Boylston has been adequately manned by only one surveyor. Figure 1 displays a matrix of 110 cells, 40 of which are randomly selected and assigned to a team of surveyors (numbering from 1 to 4 depending on the needs of the station/shift.) There are two shifts for each station and each direction. Science Park and Lechmere, being the stations near or at the end of the line, have surveyors only at the outgoing (towards Riverside) direction. The random selection of the working shifts forms the primary sampling stage. The complexity of the plan arises when only eight people are sent to the field to work in these shifts. Here the objectivity of the survey design gives way to the subjective selection of the time span within each shift



R → L -- Riverside to Lechmere
 L → R -- Lechmere (North Station)
 to Riverside

FIGURE 1. SCHEDULING OF THE PASSENGER SURVEY

based on a priori knowledge of the passenger flow at various stations and the desire to sample more heavily the busy stations and the peak hours. Each station is to be observed at one time or another and no time period is missed. The result is the survey plan delineated in Table 1, which gives Kenmore continual coverage as a point of reference to other stations.

The arrangement of labor resource, the suggestion of an optimal position from which the sampler can have a good view of the car doors, the layout of the station platform, and specific instructions during peak hours are all part of a two hour orientation/training for the samplers. Where it is difficult to count passengers at all doors (for example, during rush hours at busy stations) the samplers are to randomly select a car door for the count but systematically go to the next door of the second train when it comes around. This ensures the representativeness of the data when the counts are extrapolated to represent the entire train.

Appendix 1 is a sample of the data reported by a surveyor. Specifically, the data elements are the stations, the time of train arrival, the direction of the trip, the number of loading and unloading passengers at the car door, and the car characteristics. The samplers are also to report on other trains that pull in the station without trying to measure their loading and unloading activities, and note any unusual circumstances such as large group, train malfunction, etc.

TABLE 1. SURVEY PLAN

| Day of Week Station | Monday | Tuesday | Wednesday | Thursday | Friday |
|------------------------|--------|---------|-----------|----------|--------|
| Kenmore | AM | X | | | ⊗ |
| Auditorium | PM | | X ⊗ | | X |
| Copley | AM | X | | | |
| | PM | ⊗ | | X | |
| Arlington | AM | | | ⊗ | X |
| | PM | ⊗ | X | | ⊗ |
| Boylston | AM | | | X ⊗ | |
| | PM | X ⊗ | | | |
| Park St. | AM | ⊗ | | X | |
| | PM | | X | | ⊗ ⊗ |
| Gov't Center | AM | | | | X ⊗ |
| | PM | X | | | ⊗ |
| Haymarket | AM | X | ⊗ | | |
| | PM | X | ⊗ | | X |
| North Station | AM | | | ⊗ | X ⊗ |
| | PM | | X | | |
| Science Park | AM | | ⊗ | | |
| | PM | | | | |
| Lechmere | AM | | | | |
| | PM | | X | | ⊗ |

X Riverside to Lechmere (N.S.)

⊗ Lechmere to Riverside

To confirm the notion of nonsignificant daily variation of passenger demand, the survey design incorporates opportunities to retest that hypothesis. Samples are taken during the same time span for different days of the week at Auditorium, Arlington, and Park Street.

The design in effect offers the analyst an unreplicated discontinued time series of passenger flow for each station, unreplicated because no time periods (except those for hypothesis testing purposes) are repeated more than once, and discontinued in the sense that data gaps exist due to the labor constraint. It is the intention of Section IV, however, to attempt to fill these data gaps with an adequate statistical model and to estimate the daily trend of passenger demand with some degree of statistical confidence.

III. Data Editing

Like any other data collection activity, editing and data screening becomes an essential part of the total effort to prepare the data for analyses. Anomalies or obvious errors are to be corrected or discarded. If more than one surveyor is surveying the train, each being responsible for a car or a door, the results of each have to be combined. Or, if the combined passenger count still does not cover the entire train, extrapolation procedures are to be developed.

When the survey is completed, the data sheets are delivered to the keypunchers for the transcription of data into a file area in DEC-10. The file structure is outlined in Table 2.

TABLE 2. MBTA FILE STRUCTURE

| <u>Field Name</u> | <u>Field Description</u> | <u>Data Type</u> | <u>Length</u> |
|-------------------|--------------------------------------|------------------|---------------|
| MAYDAY | Survey date | Date | 8 |
| TIME | Time of train arrival | Integer | 4 |
| LINE | Line of train: | Text | 2 |
| | R=Riverside | | |
| | CC=Cleveland Circle | | |
| | BC=Boston College | | |
| | H=Huntington/Arborway | | |
| | K=Kenmore | | |
| | N=North Station | | |
| | L=Lechmere | | |
| | GC=Government Center | | |
| | P=Park Street | | |
| TRAIN SIZE | Number of cars in the train | Integer | 1 |
| TYPE OF CAR | LRV=Light Rail Vehicle | Text | 3 |
| | PCC=President's Conference Committee | | |
| PASSON | Number of loading passengers | Integer | 3 |
| PASSOFF | Number of unloading passengers | Integer | 3 |

TABLE 2 (CONT.)

| <u>Field Name</u> | <u>Field Description</u> | <u>Data Type</u> | <u>Length</u> |
|-------------------|--|------------------|---------------|
| CAR1 | X if car number 1 only or if the trainsize = 1, blank if otherwise | Text | 1 |
| CAR2 | X if car number 2 is counted | Text | 1 |
| CAR3 | X if car number 3 is counted | Text | 1 |
| DOOR1 | X if door is counted, blank otherwise | Text | 1 |
| DOOR2 | X if door 2 is counted, blank otherwise | Text | 1 |
| DOOR3 | X if door 3 is counted, blank otherwise | Text | 1 |
| COLLECT | Surveyor's identifier from 1 to 4 since a maximum number of 4 workers can be assigned to a shift | Integer | 1 |

In the file, each entry, representing one recording made by one surveyor has 13 fields. A series of editing programs delineated in Table 3 brings the file to its final form, with each entry representing one train observation at a station. (See Appendix 7.)

TABLE 3. EDITING PROGRAMS

| <u>Program Name</u> | <u>Function</u> | <u>Output File</u> |
|------------------------|--|---|
| EXTRAC (Appendix 3) | Extracts individual station data from the main MBTA file; such as sorts data by date and time, "ARLINGTON" or line, etc., so that the working area is reduced. It is here where data are screened manually for obvious errors. | station file "ARLINGTON" or "PARK ST" |
| EDIT (Appendix 4) | Uniquely identifies each car door whose passenger count is included in the surveyor's record. | STRAl (working file) |

TABLE 3. (CONT.)

| <u>Program Name</u> | <u>Function</u> | <u>Output File</u> |
|-------------------------|--|--|
| EDIT2 (Appendix 5) | Takes STRA1 as input, combines passenger counts from each surveyor, extrapolating if necessary, to derive total train count* | STRA2.DMI (working file) to be made into a 1022 data file. (STRA2.DMS) |
| SEPAR (Appendix 6) | Separates STRA2.DMS into 2 files according to the direction of the train (inbound or outbound) and within each file sorts the data by time. | eg. PAKLEC and PAKRIV (final data, two files for each station) (Appendix 7) |
| PROFL (Appendix 8) | Takes PAKLEC or PAKRIV and computes headways, loading and unloading rate. Also counts the number of trains between Riverside trains. | eg. PAKPFL (Riverside) and PAKPFL.NOR (North Station) or PAKPFL.LEC (Lechemere). Each file represents an average daily passenger profile (raw data) at the station. (Appendix 9) |
| CONTRA (Appendix 10) | Takes ARLPFL or ARLPPL.NOR and computes loading and unloading rates for each half hour interval. | PAKCON.RIV or PAKCON.NOR (working files) |
| COMBIN (Appendix 11) | Combines all ***CON.RIV or ***CON.NOR files into two data matrices (one for loading passenger rates and one for unloading passenger rates) with "Stations" as the Columns and "time periods" as the Rows | RIVON.MTY RIVOFF. MTY or NORON. MTY NOROFF. MTY (Table 2) |

*The extrapolating method is:

$$\text{TOTAL Train Count} = \frac{\text{total passengers count}}{\text{number of doors counted}} \times \text{total no. of doors on a train}$$

Assumes that passengers board trains equally at all doors which is not true for certain stations during certain time periods. Passengers tend to board door nearest turnstile entrance or stairwell.

The last two programs are necessary to prepare the data for input into a statistical model which synthesizes the information for all stations and all time periods to predict missing values, derives general trend for each station and estimates the average variation of passenger demand. Such a model is discussed in the next section. The matrices in Tables 4 through 7 show not only what is missing but give a bird's-eye-view of the sampling design.

IV. Survey Data Analysis

One of the assumptions underlying the sampling design is that one can pool the observations made at different days of the week to form a representative daily profile of an average week day. This assumption eliminates the necessity of obtaining sample data for each day of the week and deriving five daily profiles for each station. Previous analyses on the surface stations reflect little day to day difference in total passenger traffic. Our sampling design for the underground stations also allows for similar testing of the hypothesis. This section presents three cases in which two independent sets of passenger counts are obtained at a station during the same time span but for different days of the week. To each case, a nonparametric test, namely, the Mann-Whitney U test is applied to see if the distribution of the observations taken on Day 1 is different from those taken on Day 2.

TABLE 4. OBSERVED PASSENGER LOADING RATES AT STATIONS (TRAINS TO RIVERSIDE)

| TIME | KEN. | AUD. | COP. | ARL. | BOYL. | PARK | GOV. | HAY. | N. | SCI. | LECH. |
|------|------|------|------|------|-------|-------|-------|------|-------|------|-------|
| | | | | | | | CTR. | | STA. | PK. | |
| 700 | 0.00 | 0.00 | 0.57 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 730 | 0.00 | 0.00 | 0.73 | 0.00 | 0.00 | 3.22 | 0.00 | 2.24 | 0.00 | 0.00 | 0.00 |
| 800 | 1.00 | 0.00 | 0.82 | 3.11 | 0.00 | 8.53 | 1.35 | 4.87 | 11.68 | 0.30 | 0.00 |
| 830 | 0.19 | 0.00 | 1.14 | 2.39 | 0.00 | 13.41 | 3.75 | 2.06 | 13.19 | 0.28 | 0.00 |
| 900 | 0.53 | 0.00 | 0.00 | 0.84 | 0.00 | 0.33 | 2.81 | 5.22 | 3.90 | 0.21 | 0.00 |
| 930 | 0.10 | 0.00 | 0.00 | 0.78 | 0.00 | 4.18 | 4.73 | 0.00 | 4.80 | 0.16 | 0.00 |
| 1000 | 0.57 | 1.00 | 0.00 | 0.00 | 0.54 | 3.50 | 1.58 | 3.73 | 3.90 | 0.00 | 0.00 |
| 1030 | 0.36 | 0.38 | 0.00 | 1.15 | 0.60 | 4.57 | 1.71 | 2.22 | 0.00 | 0.00 | 0.00 |
| 1100 | 0.39 | 0.26 | 0.00 | 0.20 | 0.63 | 0.00 | 0.00 | 2.87 | 0.00 | 0.00 | 0.00 |
| 1130 | 0.48 | 0.52 | 0.00 | 0.47 | 1.11 | 0.00 | 0.00 | 0.30 | 0.00 | 0.00 | 0.00 |
| 1200 | 0.54 | 0.36 | 0.00 | 1.17 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 1230 | 0.58 | 0.00 | 3.50 | 1.12 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 1300 | 0.00 | 0.00 | 1.71 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.94 | 0.00 | 3.71 |
| 1330 | 1.05 | 0.00 | 1.57 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 3.58 |
| 1400 | 1.58 | 0.00 | 3.46 | 0.00 | 0.94 | 5.24 | 0.00 | 1.00 | 1.75 | 0.00 | 6.16 |
| 1430 | 0.69 | 0.00 | 2.00 | 0.00 | 0.77 | 4.55 | 0.00 | 1.93 | 2.77 | 0.00 | 3.47 |
| 1500 | 0.92 | 0.00 | 0.00 | 0.00 | 1.21 | 6.90 | 0.00 | 2.45 | 0.00 | 0.00 | 4.52 |
| 1530 | 0.83 | 0.00 | 0.00 | 0.00 | 0.00 | 2.33 | 0.00 | 1.69 | 0.00 | 0.00 | 5.70 |
| 1600 | 1.21 | 0.00 | 0.00 | 0.00 | 1.80 | 5.14 | 8.57 | 3.84 | 0.00 | 0.00 | 0.00 |
| 1630 | 1.06 | 0.00 | 0.00 | 0.00 | 1.28 | 7.11 | 6.25 | 1.65 | 0.00 | 0.00 | 0.00 |
| 1700 | 2.15 | 0.00 | 0.00 | 0.00 | 2.10 | 15.56 | 9.18 | 2.15 | 0.00 | 0.00 | 0.00 |
| 1730 | 2.98 | 0.00 | 0.00 | 0.00 | 1.52 | 15.23 | 12.87 | 0.00 | 0.00 | 0.00 | 0.00 |
| 1800 | 1.65 | 0.00 | 0.00 | 0.00 | 1.50 | 9.23 | 7.17 | 5.55 | 0.00 | 0.00 | 0.00 |
| 1830 | 0.81 | 0.00 | 0.00 | 0.00 | 0.00 | 0.80 | 5.63 | 0.00 | 0.00 | 0.00 | 0.00 |
| 1900 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 4.36 | 0.00 | 0.00 | 0.00 | 0.00 |
| 1930 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2000 | 0.00 | 0.00 | 0.50 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2030 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

TABLE 5. OBSERVED PASSENGER UNLOADING RATES AT STATIONS (TRAINS TO RIVERSIDE)

| TIME | KEN. | AUD. | COP. | ARL. | BOYL. | PARK | GOV. | HAY. |
|------|-------|------|------|------|-------|------|------|------|
| | | | | | | | CTR. | |
| 700 | 0.00 | 0.00 | 4.57 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 730 | 0.00 | 0.00 | 3.16 | 0.00 | 0.00 | 1.22 | 0.00 | 0.04 |
| 800 | 3.00 | 0.00 | 6.68 | 8.20 | 0.00 | 1.97 | 1.00 | 0.09 |
| 830 | 4.19 | 0.00 | 8.19 | 7.91 | 0.00 | 4.74 | 1.96 | 0.06 |
| 900 | 5.05 | 0.00 | 0.00 | 4.26 | 0.00 | 3.20 | 0.57 | 0.13 |
| 930 | 1.79 | 0.00 | 0.00 | 2.17 | 0.00 | 1.76 | 0.44 | 0.00 |
| 1000 | 1.33 | 4.33 | 0.00 | 0.00 | 0.81 | 3.25 | 0.81 | 0.00 |
| 1030 | 1.44 | 0.66 | 0.00 | 2.65 | 1.65 | 1.10 | 0.43 | 0.00 |
| 1100 | 1.78 | 0.35 | 0.00 | 0.55 | 0.20 | 0.00 | 0.00 | 0.00 |
| 1130 | 1.55 | 0.71 | 0.00 | 0.80 | 0.89 | 0.00 | 0.00 | 0.00 |
| 1200 | 1.68 | 0.73 | 0.00 | 2.63 | 0.00 | 0.00 | 0.00 | 0.00 |
| 1230 | 0.48 | 0.00 | 6.00 | 1.35 | 0.00 | 0.00 | 0.00 | 0.00 |
| 1300 | 0.00 | 0.00 | 3.03 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 1330 | 1.77 | 0.00 | 2.80 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 1400 | 2.32 | 0.00 | 3.15 | 0.00 | 0.44 | 3.48 | 0.00 | 0.24 |
| 1430 | 6.42 | 0.00 | 2.20 | 0.00 | 0.18 | 2.28 | 0.00 | 0.07 |
| 1500 | 3.81 | 0.00 | 0.00 | 0.00 | 0.34 | 1.87 | 0.00 | 0.03 |
| 1530 | 1.87 | 0.00 | 0.00 | 0.00 | 0.20 | 7.00 | 0.00 | 0.38 |
| 1600 | 2.66 | 0.00 | 0.00 | 0.00 | 2.60 | 3.38 | 0.57 | 0.00 |
| 1630 | 3.38 | 0.00 | 0.00 | 0.00 | 1.09 | 4.31 | 1.82 | 0.00 |
| 1700 | 7.38 | 0.00 | 0.00 | 0.00 | 1.34 | 8.76 | 1.05 | 0.04 |
| 1730 | 10.04 | 0.00 | 0.00 | 0.00 | 0.18 | 5.37 | 0.87 | 0.00 |
| 1800 | 8.06 | 0.00 | 0.00 | 0.00 | 0.94 | 4.00 | 0.63 | 0.50 |
| 1830 | 2.75 | 0.00 | 0.00 | 0.00 | 0.00 | 5.70 | 0.44 | 0.00 |
| 1900 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.07 | 0.00 |
| 1930 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2000 | 0.00 | 0.00 | 1.50 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2030 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

TABLE 6. OBSERVED PASSENGER LOADING RATES
AT STATIONS (TRAINS TO NORTH STATION)

| TIME | KEN. | AUD. | COP. | ARL. | BOYL. | PARK | GOV. | HAY. |
|------|------|------|------|------|-------|------|------|------|
| | | | | | | | CTR. | |
| 700 | 0.00 | 0.00 | 0.33 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 730 | 0.00 | 0.00 | 0.47 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 800 | 0.00 | 0.00 | 1.75 | 0.00 | 0.00 | 0.00 | 0.14 | 0.00 |
| 830 | 3.06 | 0.00 | 3.36 | 1.84 | 0.00 | 2.28 | 0.13 | 0.00 |
| 900 | 5.81 | 0.00 | 0.00 | 2.17 | 0.00 | 0.63 | 0.43 | 0.00 |
| 930 | 1.14 | 0.00 | 0.00 | 0.42 | 0.00 | 0.79 | 0.54 | 0.13 |
| 1000 | 0.35 | 0.96 | 0.00 | 0.00 | 0.33 | 1.21 | 0.15 | 0.00 |
| 1030 | 1.14 | 1.66 | 0.00 | 0.92 | 0.07 | 1.00 | 0.33 | 0.06 |
| 1100 | 3.29 | 1.13 | 0.94 | 1.00 | 0.16 | 0.81 | 0.94 | 0.00 |
| 1130 | 0.93 | 1.45 | 1.26 | 0.36 | 0.62 | 0.00 | 0.11 | 0.00 |
| 1200 | 1.75 | 0.00 | 0.46 | 0.56 | 0.00 | 0.00 | 0.10 | 0.00 |
| 1230 | 1.66 | 0.00 | 5.23 | 0.00 | 0.00 | 0.00 | 0.03 | 0.00 |
| 1300 | 1.11 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 1330 | 2.94 | 0.00 | 1.60 | 0.00 | 0.00 | 0.00 | 0.00 | 0.07 |
| 1400 | 3.84 | 0.00 | 2.38 | 0.00 | 0.00 | 0.00 | 0.00 | 0.04 |
| 1430 | 3.96 | 0.00 | 1.74 | 0.00 | 0.00 | 0.00 | 0.00 | 0.05 |
| 1500 | 0.00 | 0.00 | 3.11 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 1530 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 5.00 | 0.00 | 0.00 |
| 1600 | 2.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.80 | 1.30 | 0.00 |
| 1630 | 3.67 | 2.54 | 0.00 | 0.00 | 0.53 | 5.81 | 0.24 | 0.58 |
| 1700 | 2.14 | 1.36 | 0.00 | 1.58 | 1.09 | 2.18 | 0.90 | 2.22 |
| 1730 | 4.35 | 4.90 | 0.00 | 3.90 | 0.53 | 5.70 | 0.97 | 0.24 |
| 1800 | 1.08 | 1.42 | 0.00 | 2.50 | 0.08 | 1.00 | 0.72 | 0.00 |
| 1830 | 0.83 | 0.00 | 0.00 | 1.19 | 0.25 | 1.11 | 0.26 | 0.00 |
| 1900 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 1930 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2000 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2030 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

TABLE 7. OBSERVED PASSENGER UNLOADING
RATES AT STATIONS (TRAINS TO
NORTH STATION)

| TIME | KEN. | AUD. | COP. | ARL. | BOYL. | PARK | GOV. | HAY. | N. STA. |
|------|------|------|------|------|-------|-------|-------|------|------------|
| | | | | | | | CTR. | | |
| 700 | 0.00 | 0.00 | 0.47 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 730 | 0.00 | 0.00 | 0.95 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 800 | 0.00 | 0.00 | 2.69 | 0.00 | 0.00 | 22.07 | 20.43 | 0.00 | 5.15 |
| 830 | 0.50 | 0.00 | 3.96 | 3.90 | 0.00 | 10.69 | 11.65 | 0.00 | 1.09 |
| 900 | 0.38 | 0.00 | 0.00 | 4.67 | 0.00 | 13.07 | 16.97 | 0.00 | 3.53 |
| 930 | 0.59 | 0.00 | 0.00 | 2.96 | 0.00 | 5.56 | 7.15 | 0.47 | 1.09 |
| 1000 | 0.35 | 2.67 | 0.00 | 0.00 | 0.89 | 8.66 | 6.88 | 0.94 | 0.00 |
| 1030 | 0.47 | 1.45 | 0.00 | 1.46 | 0.52 | 5.11 | 2.93 | 2.22 | 0.00 |
| 1100 | 0.43 | 1.45 | 1.44 | 1.57 | 0.61 | 7.19 | 3.97 | 0.49 | 0.00 |
| 1130 | 0.00 | 0.68 | 0.85 | 0.62 | 1.12 | 0.00 | 1.14 | 0.00 | 0.00 |
| 1200 | 0.32 | 0.00 | 1.19 | 0.96 | 0.00 | 0.00 | 5.10 | 0.00 | 0.00 |
| 1230 | 0.88 | 0.00 | 1.15 | 0.00 | 0.00 | 0.00 | 4.92 | 0.00 | 0.00 |
| 1300 | 0.33 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3.56 |
| 1330 | 0.50 | 0.00 | 0.68 | 0.00 | 0.00 | 0.00 | 0.00 | 0.50 | 2.14 |
| 1400 | 1.09 | 0.00 | 2.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.39 | 1.82 |
| 1430 | 1.04 | 0.00 | 0.72 | 0.00 | 0.00 | 0.00 | 0.00 | 2.26 | 2.36 |
| 1500 | 0.00 | 0.00 | 0.86 | 0.00 | 0.00 | 0.00 | 0.00 | 3.69 | 0.00 |
| 1530 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 1600 | 0.29 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 8.17 | 5.52 | 0.00 |
| 1630 | 0.39 | 0.85 | 0.00 | 0.00 | 0.38 | 16.22 | 4.79 | 3.96 | 0.00 |
| 1700 | 0.23 | 0.71 | 0.00 | 0.50 | 0.74 | 10.30 | 4.67 | 9.04 | 0.00 |
| 1730 | 0.39 | 0.90 | 0.00 | 0.94 | 0.41 | 12.33 | 5.34 | 9.05 | 0.00 |
| 1800 | 0.50 | 0.77 | 0.00 | 0.88 | 0.46 | 7.76 | 3.62 | 3.41 | 0.00 |
| 1830 | 1.37 | 0.00 | 0.00 | 0.85 | 0.25 | 3.66 | 2.39 | 0.00 | 0.00 |
| 1900 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 1930 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2000 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2030 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

The method requires the assignment of rank w_i to each of the $n_1 + n_2$ observations according to its magnitude, where n_1 and n_2 are the total numbers of observations for Day 1 and Day 2 respectively. A U statistic is then formed by

$$U = n_1 n_2 + \frac{n_1(n_1 + 1)}{2} - \sum_{i \in \text{Day 1}} w_i$$

$$U' = n_1 n_2 + \frac{n_2(n_2 + 1)}{2} - \sum_{i \in \text{Day 2}} w_i$$

A two tailed test for the hypothesis, H_0 , that the two samples come from the same population and thus have the same distribution is as follows:

At a significance level $\alpha = .05$, H_0 is rejected if

$$\min(U, U') \leq C_{(\alpha/2, n_1, n_2)} \quad \text{or}$$

$$\min(U, U') > C_{(1-\alpha/2, n_1, n_2)}$$

where $C_{(\alpha/2, n_1, n_2)}$ is obtained from the table of critical values of U in the Mann-Whitney Test (Appendix 14) and

$$C_{(1-\alpha/2, n_1, n_2)} = n_1 n_2 - C_{(\alpha/2, n_1, n_2)}.$$

In all of the three cases in the following, the test confirms the assumption of insignificant day to day variation in the average passenger flow for the underground

stations. Along with each test result, the actual data is plotted graphically to reflect the similarity of their distributions.

Case 1: Park Street Station, 1:30pm - 3:30 pm (Figures 2 and 3).

Loading Passengers

$$U = 16 \times 16 + \frac{16(16 + 1)}{2} - 224$$

$$= 168$$

$$U' = 16 \times 16 - 224 = 88$$

$$\min(U, U') = 88$$

$$C_{\alpha/2} = 75$$

$$C_{1-\alpha/2} = 181$$

Hence $C_{\alpha/2} \leq \min(U, U') < C_{1-\alpha/2}$ and H_0 is accepted.

Unloading Passengers

$$U = 16 \times 16 + \frac{16(16 + 1)}{2} - 279.50 = 112.50$$

$$U' = 16 \times 16 - 112.50 = 143.50$$

$$\min(U, U') = 112.50$$

$$C_{(\alpha/2, n_1, n_2)} = 75$$

$$C_{(1-\alpha/2, n_1, n_2)} = 181$$

Hence $C_{(1-\alpha/2, n_1, n_2)} \leq \min(U, U') < C_{(\alpha/2, n_1, n_2)}$

and H_0 is accepted.

FRIDAY

THURSDAY

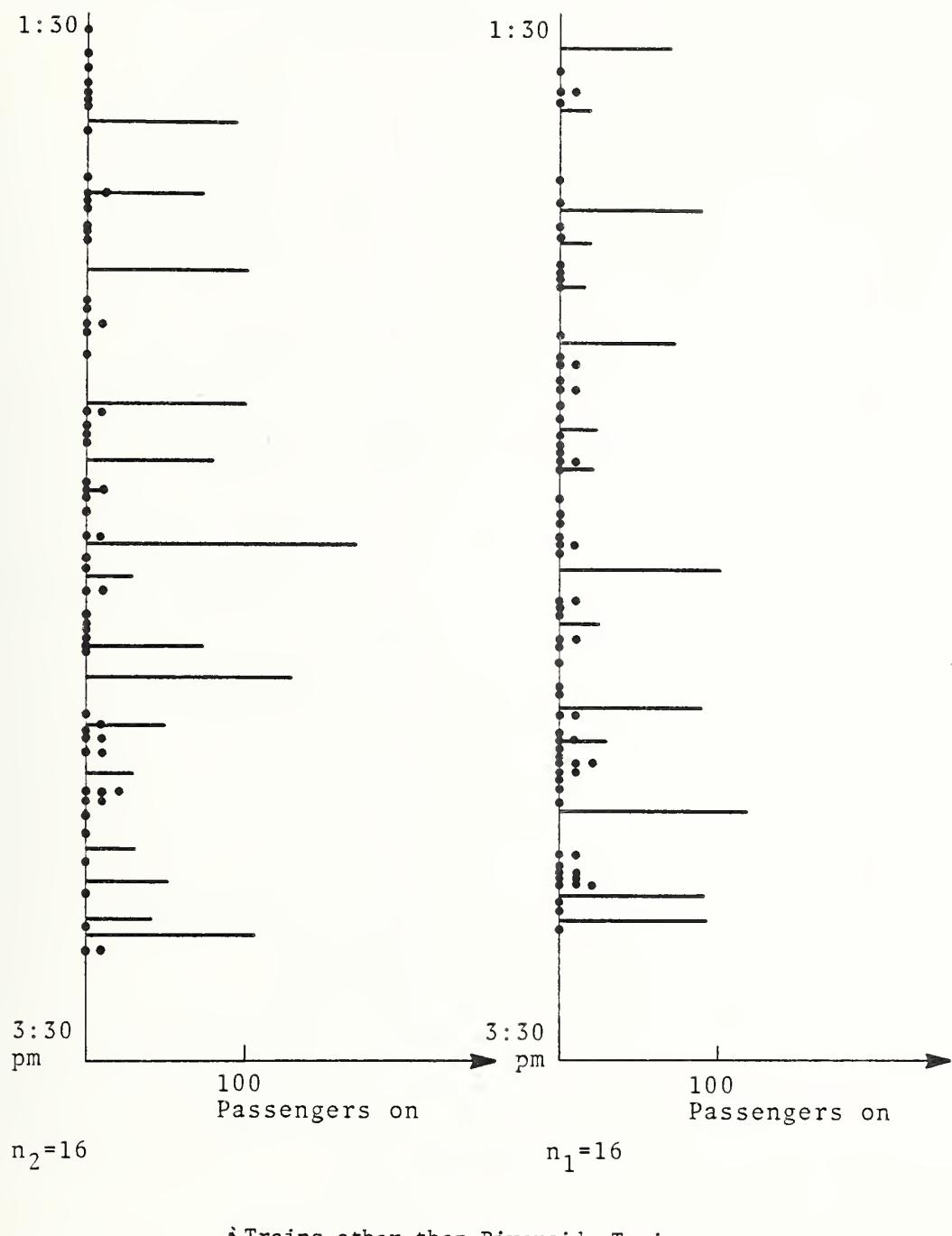


FIGURE 2. DISTRIBUTION OF LOADING PASSENGERS: CASE 1

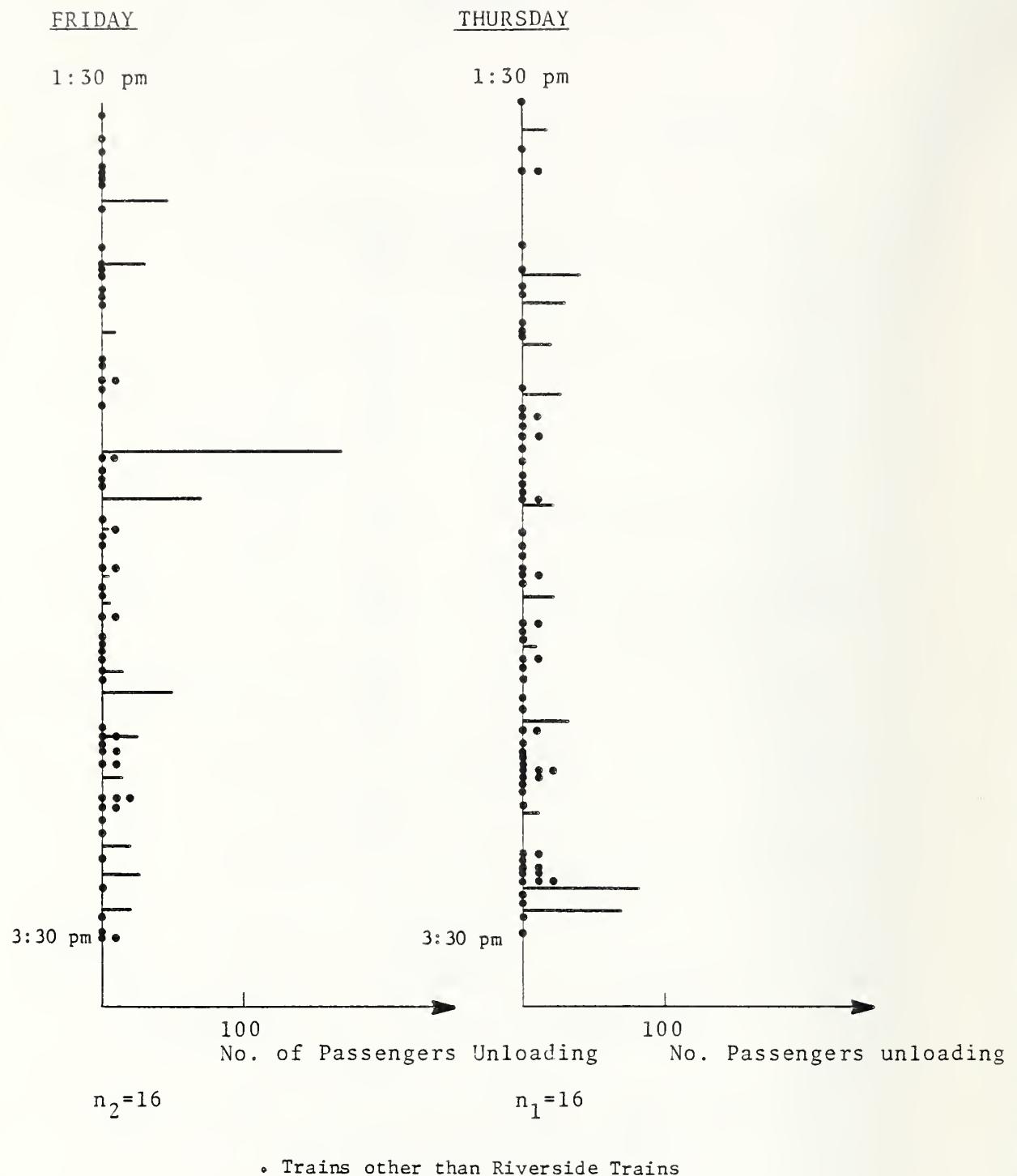


FIGURE 3. DISTRIBUTION OF UNLOADING PASSENGERS: CASE 1

Case 2: Auditorium Station, 10:00 am - 12:00 pm (Figures 4 and 5).

Loading Passengers

$$U = 10 \times 13 + \frac{10(10 + 1)}{2} - 116.5$$

$$= 68.50$$

$$U' = 61.50$$

$$\min (U, U') = 61.50$$

$$C_{(\alpha/2, n_1, n_2)} = 33$$

$$C_{(1-\alpha/2, n_1, n_2)} = 97$$

$$\text{Hence } C_{(\alpha/2, n_1, n_2)} \leq \min (U, U') < C_{(1-\alpha/2, n_1, n_2)}$$

and H_0 is accepted.

Unloading Passengers

$$U = 10 \times 13 + \frac{10(10 + 1)}{2} - 118$$

$$= 67$$

$$U' = 63$$

$$\min (U, U') = 63$$

$$C_{(\alpha/2, n_1, n_2)} = 33$$

$$C_{(1-\alpha/2, n_1, n_2)} = 97$$

$$\text{Hence } C_{(1-\alpha, n_1, n_2)} \leq \min (U, U') < C_{(1-\alpha/2, n_1, n_2)}$$

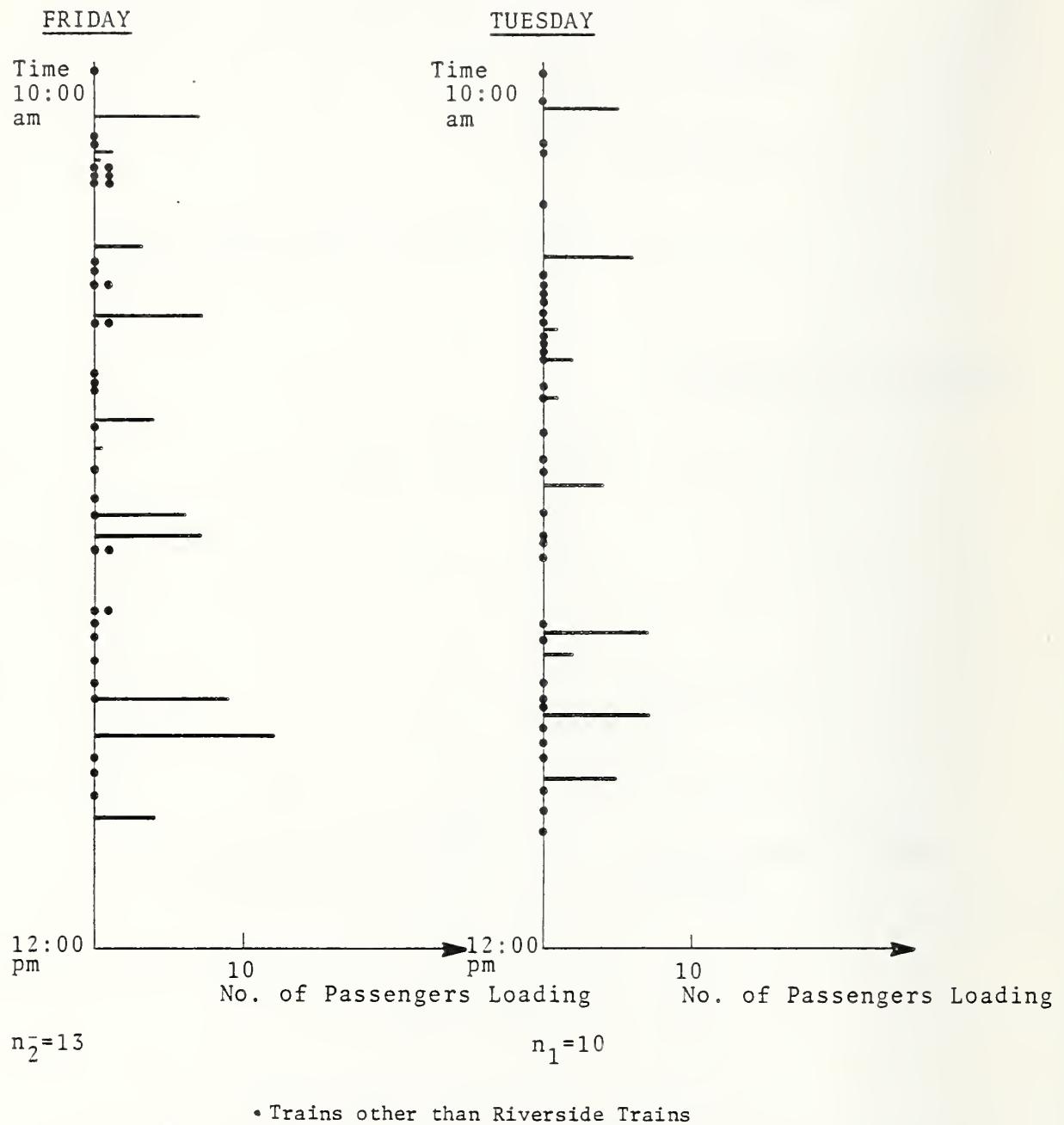


FIGURE 4. DISTRIBUTION OF LOADING PASSENGERS: CASE 2

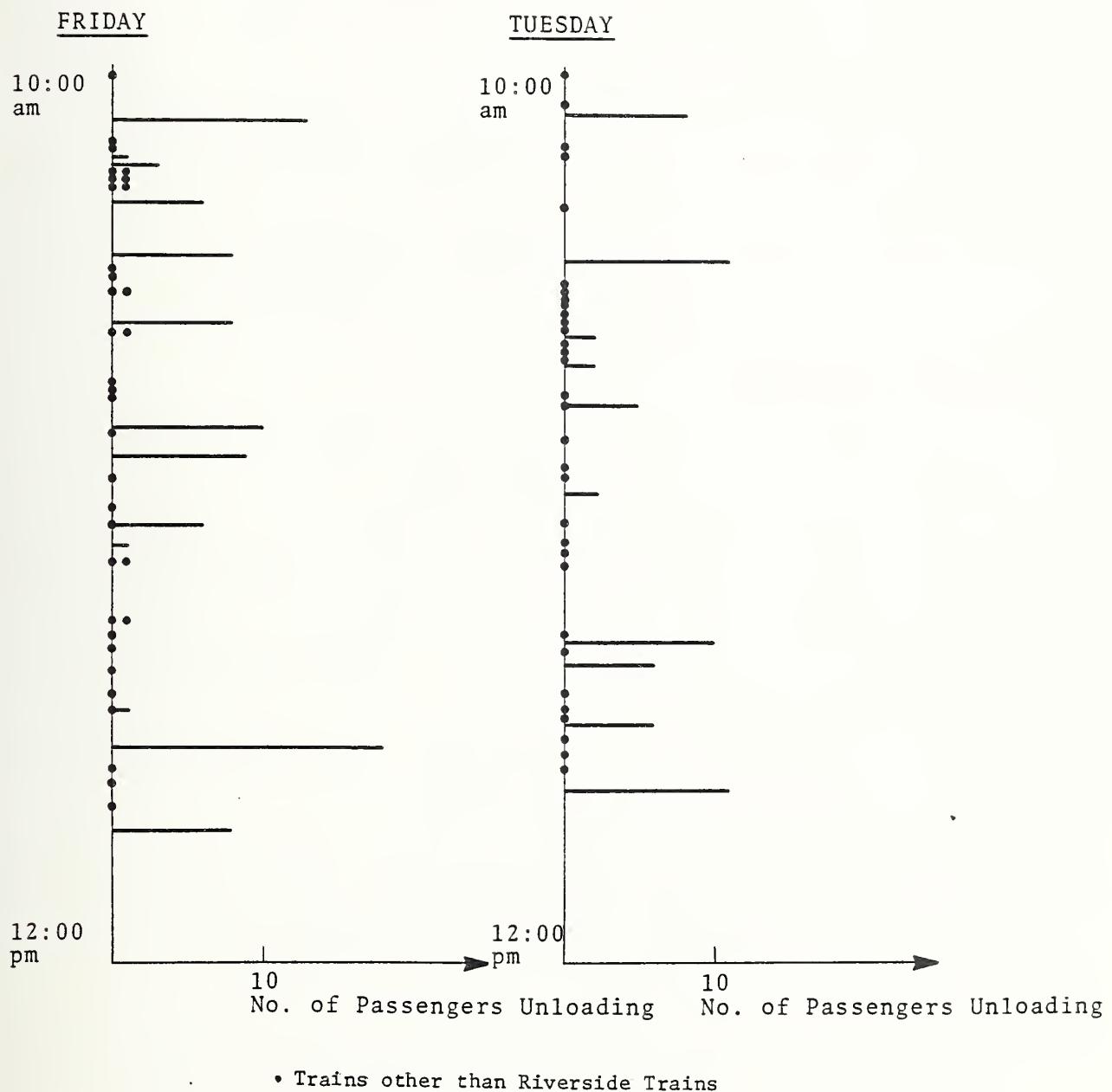


FIGURE 5. DISTRIBUTION OF UNLOADING PASSENGERS: CASE 2

Case 3: Arlington Station, 10:00 am - 12:00 pm (Figures 6 and 7)

$$U = 8 \times 11 + \frac{8(8 + 1)}{2} - 74 \\ = 50$$

$$U' = 8 \times 11 - 50 = 38$$

$$\min(U, U') = 38$$

$$C_{(\alpha/2, n_1, n_2)} = 19$$

$$C_{(1-\alpha/2, n_1, n_2)} = 69$$

$$\text{Hence } C_{(\alpha/2, n_1, n_2)} \leq \min(U, U') < C_{(1-\alpha/2, n_1, n_2)}$$

and H_0 is accepted.

Unloading Passengers

$$U = 8 \times 11 + \frac{8(8 + 1)}{2} - 89 \\ = 35$$

$$U' = 8 \times 11 - 35 = 53$$

$$\min(U, U') = 35$$

$$C_{(\alpha/2, n_1, n_2)} = 19$$

$$C_{(1-\alpha/2, n_1, n_2)} = 69$$

$$\text{Hence } C_{(\alpha/2, n_1, n_2)} < \min(U, U') < C_{(1-\alpha/2, n_1, n_2)}$$

and H_0 is accepted.

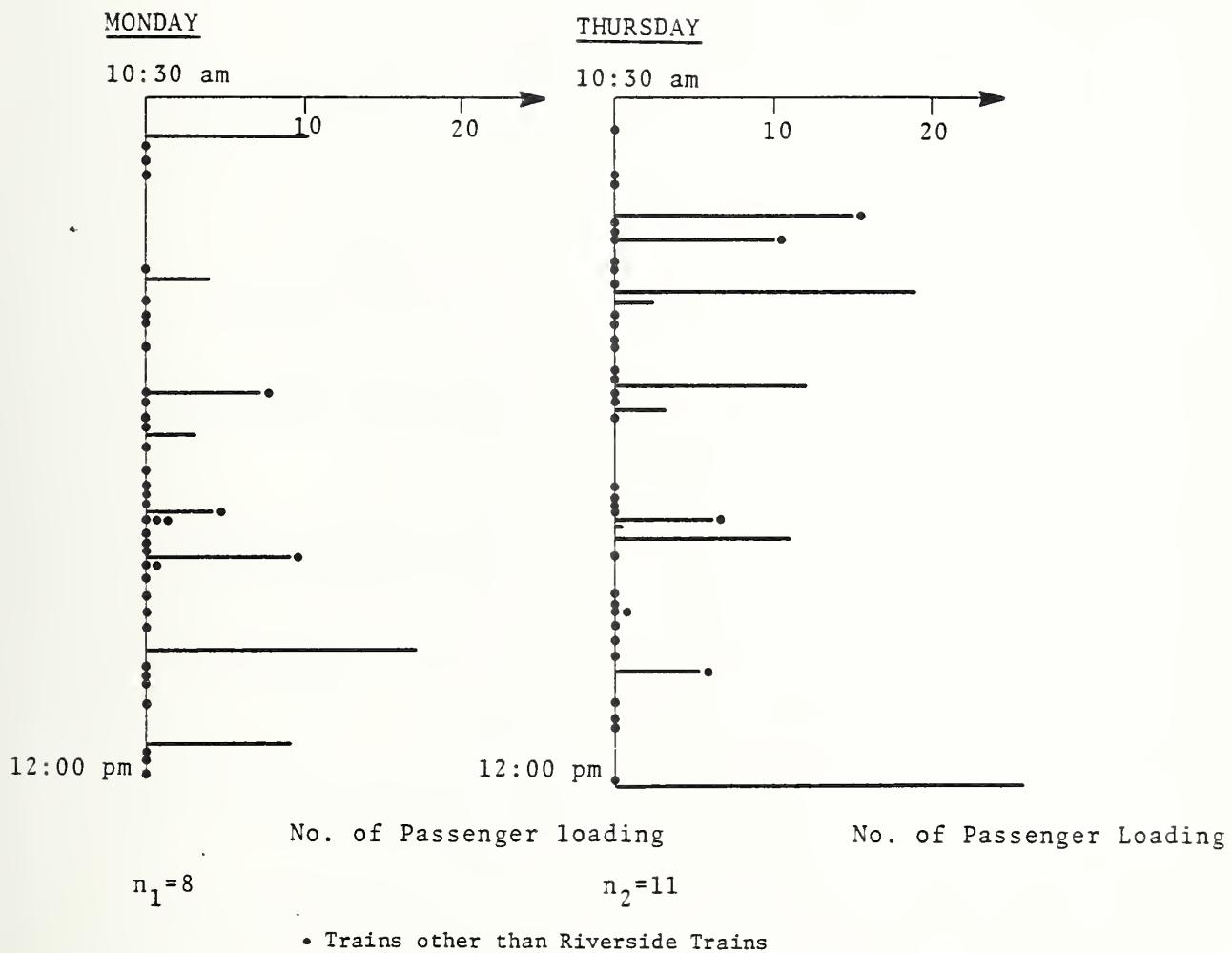
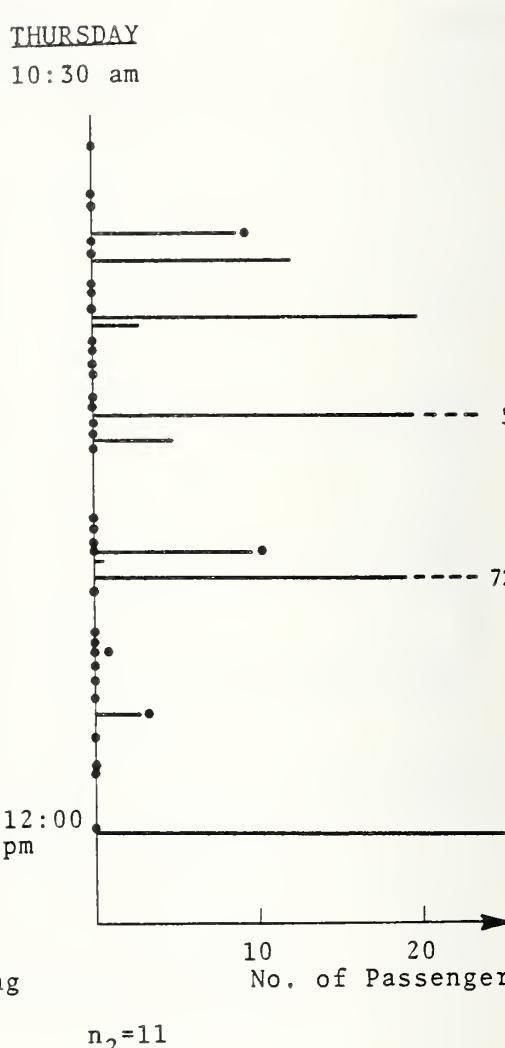
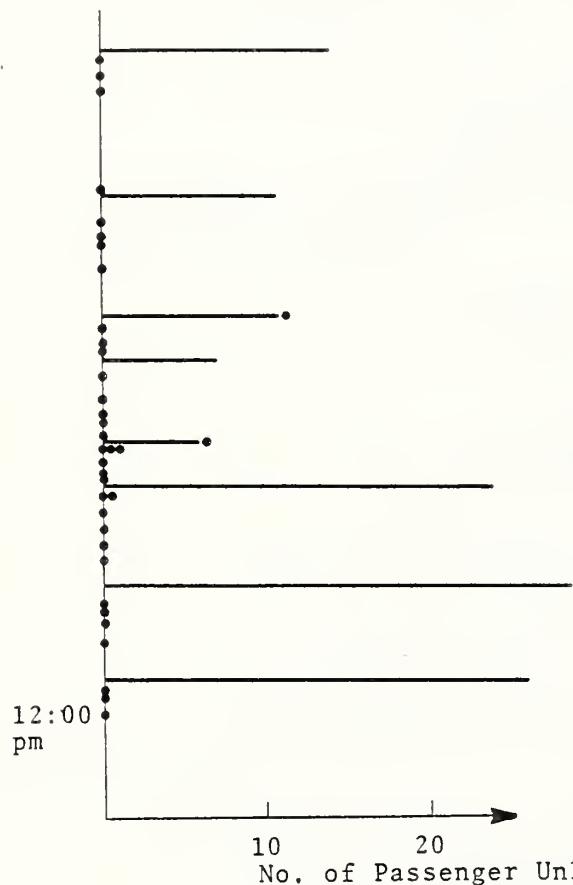


FIGURE 6. DISTRIBUTION OF LOADING PASSENGERS: CASE 3

MONDAY

10:30 am



V. Statistical Model to Predict Data Gaps

A. Background

Tables 4 through 7 show four two dimensional matrices with "station" as columns and "time period" as rows. The half hourly periods are used for two reasons. First, a uniform time scale is required for all stations if all the information is pooled together in the statistical model such that a prediction of passenger demand at Park Street, for example, will depend on the knowledge of passenger demand for the same time span at other stations. Secondly, because of the variable headways of the train arrival, a thirty-minute interval is the smallest time interval for which a meaningful estimate of average passenger arrival rate can be obtained. Cutting the interval into anything smaller would introduce too many data gaps.

Hence Tables 4 through 7 in fact present four matrices containing the average passenger rate of flow for each time period and each station, on each of which a two-factor analysis of variance can be performed, a technique that investigates the simultaneous effects of two factors, namely "station" and "time" on the response cell, the passenger loading and unloading rate. That is, if we designate R_{IJ} be the average passenger rate for station J and time period I, R_{IJ} can be expressed as a sum of five components:

$$R_{IJK} = \mu + \alpha_I + \beta + (\alpha\beta)_{IJ} + \varepsilon_{IJK} \quad (1)$$

where μ is the grand mean, α_I , the effect contributed by time period I, β_J the effect contributed by station J, $(\alpha\beta)_{IJ}$ the effect contributed by the interaction between station I and time J, and ϵ_{IJK} the random error term.

Certain constraints are placed on Model (1). They are:

$$\sum_I \alpha_I = 0, \quad \sum_J \beta_J = 0, \quad \sum_I (\alpha\beta)_{IJ} = 0, \quad \sum_J (\alpha\beta)_{IJ} = 0$$

ϵ_{IJK} 's are uncorrelated with mean zero and variance σ^2 .

This model is generally called a "fixed effect" two-way ANOVA since the factor levels I and J are of intrinsic interest themselves. If all the constraints are satisfied, R_{IJK} are then independently distributed as $N(\mu + \alpha_I + \beta_J + (\alpha\beta)_{IJ}, \sigma^2)$.

B. Modification of Model (1)

Model (1) will be modified as follows:

- o assumption of unimportant interaction effects, or,
for all I,J pairs, $(\alpha\beta)_{IJ} = 0$
- o application of a generalized linear model because of
missing data or empty cells.

Table application of a straightforward two-way ANOVA to the matrices in Tables 4 through 7 seems simple enough. However, there is at most only one observation per cell (i.e. $K = 1$), not to mention the empty cells for which data is lacking and the prediction of which is precisely the objective this model set out to fulfill. Having one observation per cell

implies the infeasibility of estimating the error term without assuming the interaction effect $(\alpha\beta)_{IJ}$ be zero or insignificant. Empty cells make it inappropriate to use any standard ANOVA statistical computer package which usually requires balanced data (i.e. equal sample size per cell).

Setting $(\alpha\beta)_{IJ} = 0$, Model (1) then becomes:

$$R_{IJ} = \mu + \alpha_I + \beta_J + \epsilon_{IJ} \quad (1.a)$$

a) Regression Approach to the Analysis of Variance Problem

When the cells of the ANOVA matrix have unequal sample sizes or empty cells, the regular ANOVA equations are no longer of a simple structure. The best alternative is to re-express the ANOVA model by its regression model counterpart. In formulating the regression model, we use indicator variables to represent the "station" effects and the "time" effects. Specifically we have:

$$R_{IJ} = \mu + \sum_i a_i T_i + \sum_j b_j S_j + \epsilon_{IJ} \quad (2)$$

where T_i and S_j are defined as:

$$\begin{aligned} T_i &= 1 && \text{if } i = I \text{ and } I \neq t \\ &= -1 && \text{for all } i \text{ if } I = t \\ &= 0 && \text{otherwise} \end{aligned}$$

$s_j = 1$ if $j = J$ and $J \neq s$
 $= -1$ for all j if $J = s$
 $= 0$ otherwise

for all $i = 1, 2, 3, \dots, t-1, t$ being the number of time

periods

and $j = 1, 2, 3, \dots, s-1, s$ being the number of stations

μ, a_i, b_j are parameters to be estimated, and ε_{IJ} the usual random error term; ε_{IJ} are uncorrelated with mean $E(\varepsilon_{IJ}) = 0$ and variance $v(\varepsilon_{IJ}) = \sigma^2$.

We note that the regression approach (Model (2)) gives rise to the same result as the ANOVA Model (1.a). The indicator variables are coded in such a way that their regression coefficients correspond directly to the level effects in Model (1.a). To illustrate, for a particular I, J pair, $I \neq t$ and $J \neq s$,

Model (1.a) gives: $R_{IJ} = \mu + \alpha_I + \beta_J + \varepsilon_{IJ}$

Model (2) gives: $R_{IJ} = u + a_I + b_J + \varepsilon_{IJ}$.

For $I = t$ and $J = s$,

Model (1.a) gives: $R_{ts} = \mu + \alpha_t + \beta_s + \varepsilon_{ts}$

Model (2) gives: $R_{ts} = u - \sum_i a_i - \sum_j b_j + \varepsilon_{ts}$

$i = 1, \dots, t-1$ and
 $j = 1, \dots, s-1$.

If one equates R_{IJ} of Model (1.a) to that of Model (2), the set of simultaneous equations will result in the following identities:

$$\mu = u$$

$$\alpha_I = a_I \quad \text{for all } I \neq t$$

$$\alpha_t = - \sum_i a_i = a_t \quad i = 1, \dots, t-1$$

$$\beta_J = b_J \quad \text{for all } J \neq s$$

$$\beta_s = - \sum_j b_j = b_s \quad j = 1, \dots, s-1$$

Still the regression approach assumes the interaction effect is insignificant because the addition of interaction variable, $(TS)_{ij}$, for all possible i, j pairs, makes the equation cumbersome. Moreover, the number of observations available may not support the estimation of the vast number of parameters (or regression coefficients). From the analysis on surface station data, we are shown that each surface station has a constant market share of passenger demand during each time period. For the underground stations, however, many of which are transfer points such as Park Street, Government Center, Haymarket, and North Station, additional evidence about the assumption is necessary.

b) Tukey One Degree of Freedom Test for Interaction

Tukey postulated that, in an ANOVA model, if $(\alpha\beta)_{IJ}$ is any second degree polynomial function of α_I and β_J , then the interaction term would be in the form:

$$(\alpha\beta)_{IJ} = D\alpha_I\beta_J$$

for some constant D, to satisfy the constraints set forth under Model (1). The interaction sum of squares, SSAB, will be:

$$SSAB = \sum_I \sum_J (\alpha\beta)_{IJ}^2 = \sum_I \sum_J D^2 \alpha_I^2 \beta_J^2$$

Assuming α_I , β_J are known, the least square estimator of D is:

$$D = \frac{\sum_I \sum_J \alpha_I \beta_J R_{IJ}}{\sum_I \alpha_I^2 \sum_J \beta_J^2} \quad I = 1, \dots, t, \quad J = 1, \dots, s.$$

The test statistic for interaction, FSTAT, when only one observation per cell is available, is then a function of the approximate sum of squares for interaction (SSAB) and the sum of squares of error (SSE).

$$FSTAT = \frac{SSAB}{1} \left/ \frac{(SSE - SSAB)}{(df \text{ for } SSE - 1)} \right.$$

It is important in our estimation of the distribution of the passenger demand to assure the correctness of all the assumptions we have set forth in the beginning. Our hypothesis is:

H_0 = Constant market shares for underground stations,
no interaction between "station" and "time".

H_1 = Interaction exists. A particular station at a particular time may have unusually heavy or light traffic than what other stations normally call for.

The test statistic FSTAT is distributed $F(1, df(SSE)-1)$, and large values of FSTAT would lead to conclusion H_1 .

C. Presentation of Results

It is intended in this section to dwell on the regression results of the input matrix from Table 4 in detail and briefly discuss the others since similar analyses are performed on each of them. Table 8 presents the regression results on RIVON.MTY. There are $t = 25$ time periods and $s = 11$ stations, making the number of parameters $(25-1) + (11-1) = 34$ plus an intercept term. The total number of observations (loading passenger rate) is $n=120$.

An examination of Table 8 reveals the following facts about the aptness' of the Model (2) when applied to this set of data:

- o The regression shows an F value of 6.78 which, when compared to an $f(24.85)$ at a significance level of $\alpha = .05$, is highly significant. The multiple

TABLE 8. ANOVA RESULTS ON RIVON.MTY: MODEL (2) ANALYSIS OF VARIANCE FOR THE REGRESSION (UNTRANSFORMED DATA)

| SOURCE OF VARIATION | DF | SUM OF SQUARE | MEAN SQUARE | F-VALUE |
|----------------------------|-----|---------------|-------------|---------|
| ATTRIBUTABLE TO REGRESSION | 34. | 1028.2714 | 30.2433 | 6.7834 |
| DEVIATION FROM REGRESSION | 85. | 378.9656 | 4.4584 | |

INTERCLPT= 2.975
 MULTIPLE CORR. COEFF.= .85481 $R^2 = .73$
 STANDARD ERROR OF ESTIMATE= 2.111

| VARIABLE | REGR. COEFF. | STD. ERROR, OF COEFF. | COMPUTED T-VALUE |
|----------|--------------|--------------------------|---------------------|
| 2 | -1.9401 | 2.1768 | -0.8913 |
| 3 | -2.2433 | 1.2277 | -1.8273 |
| 4 | 0.7824 | 0.7692 | 1.0173 |
| 5 | 1.6262 | 0.7692 | 2.1143 |
| 6 | -0.4358 | 0.8249 | -0.5283 |
| 7 | -0.8862 | 0.8929 | -0.9925 |
| 8 | -1.2497 | 0.8169 | -1.5298 |
| 9 | -1.1731 | 0.8204 | -1.4300 |
| 10 | -0.4986 | 0.9767 | -0.5105 |
| 11 | -0.3600 | 1.0977 | -0.3279 |
| 12 | -0.3913 | 1.2728 | -0.3074 |
| 13 | 0.2282 | 1.2353 | 0.1847 |
| 14 | -1.7326 | 1.2827 | -1.3508 |
| 15 | -1.7481 | 1.0932 | -1.5991 |
| 16 | -0.7497 | 0.8170 | -0.9177 |
| 17 | -1.3140 | 0.8170 | -1.6084 |
| 18 | -0.2261 | 0.9615 | -0.2352 |
| 19 | 1.0489 | 1.0724 | 0.9781 |
| 20 | 0.7936 | 0.9520 | 0.8336 |
| 21 | 0.1516 | 0.9520 | 0.1592 |
| 22 | 2.9096 | 0.9520 | 3.0563 |
| 23 | 4.7028 | 1.0614 | 4.4305 |
| 24 | 1.7016 | 0.9520 | 1.7874 |
| 25 | 1.4157 | 1.2179 | 1.1624 |
| 26 | -2.3406 | 0.4822 | -4.8540 |
| 27 | -1.7365 | 0.9928 | -1.7491 |
| 28 | -0.4649 | 0.7845 | -0.5926 |
| 29 | -1.6041 | 0.7266 | -2.2078 |
| 30 | -2.1990 | 0.6375 | -3.4492 |
| 31 | 4.6118 | 0.5378 | 8.5759 |
| 32 | 1.7968 | 0.6360 | 2.8252 |
| 33 | -0.1519 | 0.5641 | -0.2693 |
| 34 | 2.7625 | 0.7123 | 3.8784 |
| 35 | -3.0092 | 1.0478 | -2.8718 |

THE INTERACTION TEST STAT. , FSTAT1 78.1136

| ORIG. RATE | FITTED RATE | RESIDUAL | STAND. RES. |
|------------|-------------|----------|-------------|
| 0.00 | -1.31 | 1.31 | 0.62 |
| 0.00 | -0.70 | 0.70 | 0.33 |
| 0.57 | 0.57 | 0.00 | 0.00 |
| 0.00 | -0.57 | 0.57 | 0.27 |

correlation coefficient $R^2 = .73$ indicates that the regression has explained about 73% of the variation in the passenger data.

- o Small t values are attached to some of the regression coefficients showing some stations or time periods have similar mean levels of passenger traffic. The usual approach of eliminating an insignificant variable does not apply when the objective is not determining the correlation between variables, but rather the estimation of level means.
- o The FSTAT statistic for testing interaction between the station factor and the time factor is disturbingly large (FSAT = 78.11). At any significance level, it is concluded that our assumption of $(\alpha\beta)_{IJ} = 0$ in Model (1.a) is not justified. To remove the existing interaction, a transformation of the data may prove useful.

By examining the residuals, ϵ_{IJ} , additional information can be obtained and the aptness of the model determined.

- o Figure 8 shows a plot of the residuals, ϵ_{IJ} , vs. the fitted values, \hat{R}_{IJ} . It reveals a gradual increase in the variation of the residuals around the expected mean $E(\epsilon_{IJ}) = 0$. As the value of \hat{R}_{IJ} increases, so also does the deviation from the mean. Heteroschedasity, or unequal variance in the residuals, is apparent.

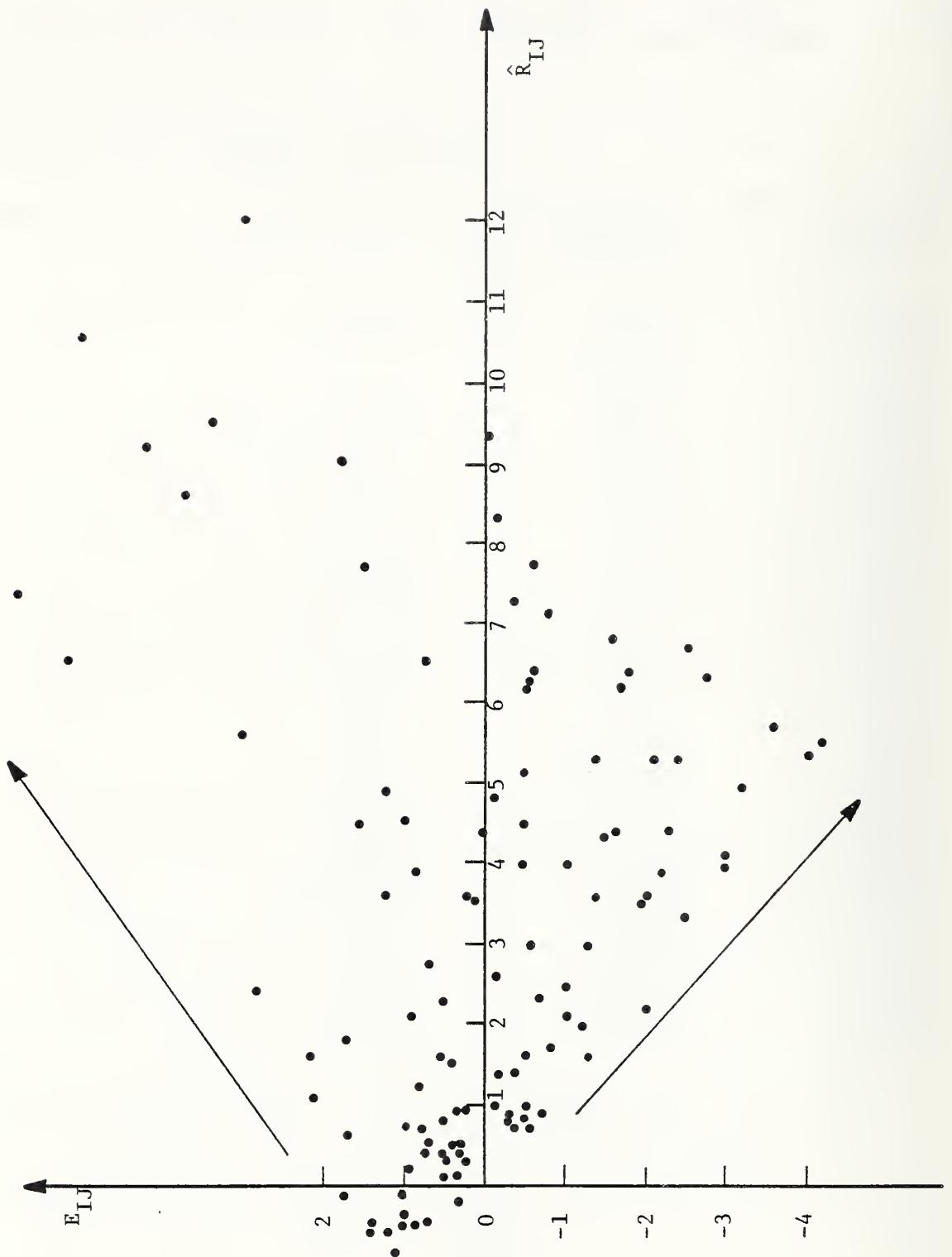


FIGURE 8. PLOT OF THE RESIDUALS, E_{IJ} , VS. THE PREDICTED VALUE, \hat{R}_{IJ}

- o Figure 9 shows a normal probability plot of ϵ_{IJ} , in which the cumulative distribution of the standardized residuals is compared against that of a standard normal distribution, $N(0,1)$. Again, it shows a slight departure from the normality assumption near the lower end of the scale. As normality is a rather robust condition, a slight departure will not hinder the effectiveness of the model.

Figure 10 plots the fitted values, \hat{R}_{IJ} , against the original values R_{IJ} . This is done in an attempt to detect any systematic departure of the existing model from the true model. A random distribution of the points around the line $\hat{R}_{IJ} = R_{IJ}$ will give credence that the regression model (2) is indeed suitable. We notice, however, that for the lower values, the \hat{R}_{IJ} 's are usually greater than the R_{IJ} 's and the pattern is reverse for the higher values. We are led to believe then that \hat{R}_{IJ} is some function of R_{IJ} and a transformation of the data is necessary to straighten the curve.

Transformation of data to improve Model (2)

Based on the information gleaned from the residual plots and ANOVA results above, a modification of the Model (2) is necessary. Transformation of the data serves several objectives:

- o to stabilize the variance of the residuals,
- o to improve the normality of the residuals,
- o to improve the fitness of the model,

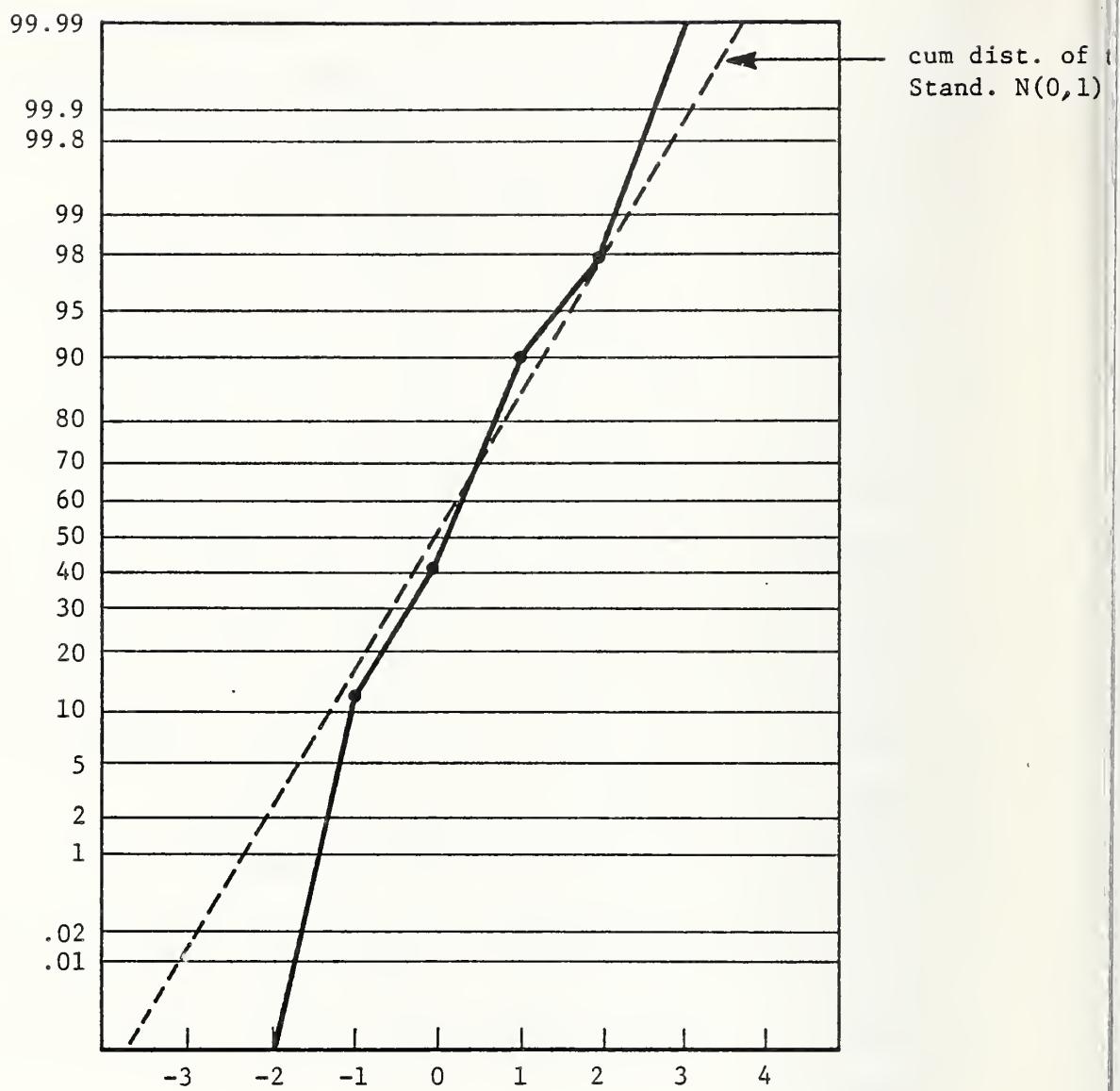
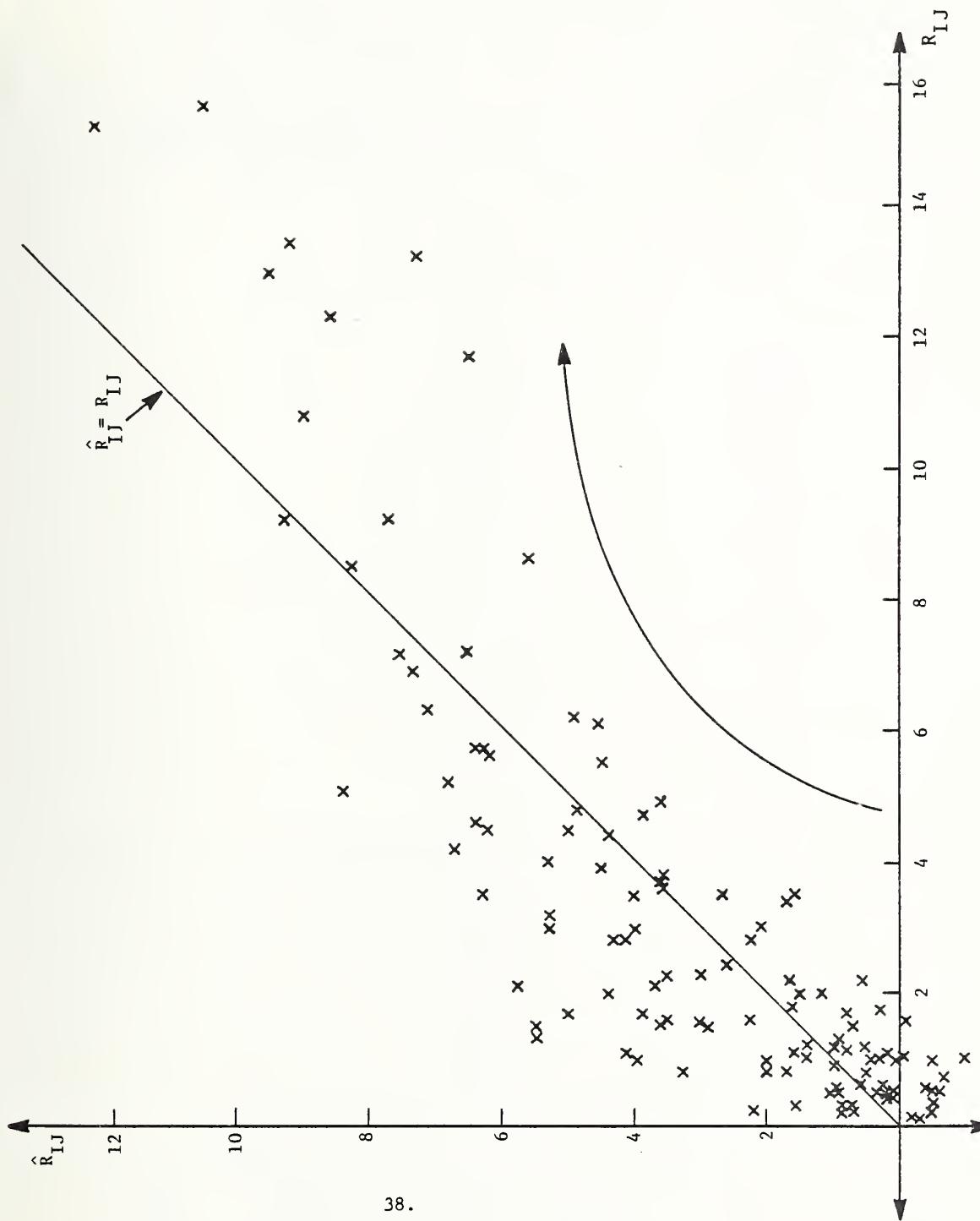


FIGURE 9. NORMALITY PLOT OF THE STANDARDIZED RESIDUALS (UNTRANSFORMED DATA)



38.

37

FIGURE 10. PLOT OF PREDICTED VALUES, \hat{R}_{IJ} , VS. THE ACTUAL, R_{IJ} (UNTRANSFORMED DATA)

- o to remove or minimize the interaction effect between the station factor and the time factor.

By examining Figure 10, a logarithmic transformation $\tilde{R}_{IJ} = \log_e R_{IJ}$, for all pairs seems appropriate. Model (2) thus becomes:

$$\log_e R_{IJ} = u + \sum_i a_i T_i + \sum_j b_j S_j + \varepsilon_{IJ} \quad (3)$$

Or, equivalently,

$$R_{IJ} = \prod_i \prod_j v c_i^{T_i} d_j^{S_j} \eta_{IJ}$$

$$\text{where } u = \log v, a_i = \log c_i, b_j = \log d_j$$

$$\varepsilon_{IJ} = \log \eta_{IJ}$$

$$i = 1, \dots, t-1; j = 1, 2, \dots, s-1$$

$$I = 1, \dots, t \quad J = 1, \dots, s$$

It is gratifying to see the improvements in the subsequent regression results of Model (3), which are presented in Table 9. The F statistic (which indicates the statistical significance of the model) has increased from 6.78 to 11.83. The multiple correlation coefficient square shows that the new regression explains about 83% (compared to 73%) of the data variation. The FSTAT has dramatically fallen from 78.11 to a low 4.09. Moreover, the residual plots (Figures 11 - 13) all verify the assumption that Model (3) is based

TABLE 9. ANOVA RESULTS OF RIVON.MTY: MODEL (3) ANALYSIS OF VARIANCE FOR THE REGRESSION (TRANSFORMED DATA)

| SOURCE OF VARIATION | DF | SUM OF SQUARE | MEAN SQUARE | F-VALUE |
|----------------------------|-----|---------------|-------------|---------|
| ATTRIBUTABLE TO REGRESSION | 34. | 123.3282 | 3.6273 | 11.8273 |
| DEVIATION FROM REGRESSION | 85. | 26.0686 | 0.3067 | |

INTERCEPT= 0.481
 MULTIPLE CORR. COEFF. SQUARE=.82551
 STANDARD ERROR OF ESTIMATE= 0.554

| VARIABLE | REGR. COEFF. | STD. ERROR, OF COEFF. | COMPUTED T-VALUE |
|----------|--------------|--------------------------|---------------------|
| 2 | -0.1209 | 0.5709 | -1.9634 |
| 3 | -0.5345 | 0.3220 | -1.6599 |
| 4 | 0.2494 | 0.2017 | 1.2364 |
| 5 | 0.1868 | 0.2017 | 0.9260 |
| 6 | -0.0201 | 0.2163 | -0.0929 |
| 7 | -0.4322 | 0.2342 | -1.8456 |
| 8 | -0.1861 | 0.2143 | -0.8686 |
| 9 | -0.3863 | 0.2152 | -1.7954 |
| 10 | -0.6878 | 0.2562 | -2.6848 |
| 11 | -0.3178 | 0.2879 | -1.1040 |
| 12 | -0.2577 | 0.3338 | -0.7719 |
| 13 | 0.1798 | 0.3240 | 0.5550 |
| 14 | -0.2097 | 0.3364 | -0.6234 |
| 15 | -0.3448 | 0.2867 | -1.2026 |
| 16 | -0.0186 | 0.2143 | -0.0866 |
| 17 | -0.1863 | 0.2143 | -0.8696 |
| 18 | 0.1280 | 0.2522 | 0.5076 |
| 19 | 0.1820 | 0.2813 | 0.6471 |
| 20 | 0.4810 | 0.2497 | 1.9262 |
| 21 | 0.2191 | 0.2497 | 0.8775 |
| 22 | 0.7460 | 0.2497 | 2.9878 |
| 23 | 1.0444 | 0.2784 | 3.7517 |
| 24 | 0.6616 | 0.2497 | 2.6497 |
| 25 | 0.4111 | 0.3194 | 1.2869 |
| 26 | -0.8815 | 0.1265 | -6.9701 |
| 27 | -0.9117 | 0.2604 | -3.5014 |
| 28 | 0.0780 | 0.2057 | 0.3791 |
| 29 | -0.3570 | 0.1906 | -1.8732 |
| 30 | -0.5403 | 0.1672 | -3.2313 |
| 31 | 1.3248 | 0.1410 | 9.3927 |
| 32 | 0.7781 | 0.1668 | 4.6645 |
| 33 | 0.4194 | 0.1479 | 2.8344 |
| 34 | 0.9577 | 0.1868 | 5.1263 |
| 35 | -1.9443 | 0.2748 | -7.0749 |

THE INTERACTION TEST STAT. , FSTAT: 4.0902

| ORIG. RATE | FITTED RATE | RESIDUAL | STAND. RES. |
|------------|-------------|----------|-------------|
| 0.00 | 0.22 | 0.00 | 0.00 |
| 0.00 | 0.21 | 0.00 | 0.00 |
| 0.57 | 0.57 | 0.00 | 0.00 |
| 0.00 | 0.37 | 0.00 | 0.00 |

TABLE 9. (CONT.)

| ORIG. RATE | FITTED RATE | RESIDUAL | STAND. RES. |
|------------|-------------|----------|-------------|
| 0.00 | 7.28 | 0.00 | 0.00 |
| 0.00 | 4.22 | 0.00 | 0.00 |
| 0.00 | 2.94 | 0.00 | 0.00 |
| 0.00 | 5.04 | 0.00 | 0.00 |
| 0.00 | 0.28 | 0.00 | 0.00 |
| 0.00 | 5.68 | 0.00 | 0.00 |
| 0.00 | 0.54 | 0.00 | 0.00 |
| 0.00 | 0.53 | 0.00 | 0.00 |
| 1.71 | 1.42 | 0.19 | 0.34 |
| 0.00 | 0.92 | 0.00 | 0.00 |
| 0.00 | 0.76 | 0.00 | 0.00 |
| 0.00 | 4.93 | 0.00 | 0.00 |
| 0.00 | 2.86 | 0.00 | 0.00 |
| 0.00 | 1.99 | 0.00 | 0.00 |
| 2.94 | 3.42 | -0.15 | -0.27 |
| 0.00 | 0.19 | 0.00 | 0.00 |
| 3.71 | 3.85 | -0.04 | -0.07 |
| 1.05 | 0.47 | 0.79 | 1.43 |
| 0.00 | 0.46 | 0.00 | 0.00 |
| 1.57 | 1.24 | 0.24 | 0.43 |
| 0.00 | 0.80 | 0.00 | 0.00 |
| 0.00 | 0.67 | 0.00 | 0.00 |
| 0.00 | 4.31 | 0.00 | 0.00 |
| 0.00 | 2.49 | 0.00 | 0.00 |
| 0.00 | 1.74 | 0.00 | 0.00 |
| 1.00 | 2.99 | -1.09 | -1.97 |
| 0.00 | 0.16 | 0.00 | 0.00 |
| 3.58 | 3.36 | 0.06 | 0.11 |
| 1.58 | 0.66 | 0.88 | 1.58 |
| 0.00 | 0.64 | 0.00 | 0.00 |
| 3.46 | 1.72 | 0.70 | 1.27 |
| 0.00 | 1.11 | 0.00 | 0.00 |
| 0.94 | 0.92 | 0.02 | 0.03 |
| 5.24 | 5.97 | -0.13 | -0.24 |
| 0.00 | 3.46 | 0.00 | 0.00 |
| 1.00 | 2.41 | -0.88 | -1.59 |
| 1.75 | 4.14 | -0.86 | -1.55 |
| 0.00 | 0.23 | 0.00 | 0.00 |
| 6.10 | 4.66 | 0.28 | 0.50 |
| 0.69 | 0.56 | 0.22 | 0.39 |
| 0.00 | 0.54 | 0.00 | 0.00 |
| 2.00 | 1.45 | 0.32 | 0.58 |
| 0.00 | 0.94 | 0.00 | 0.00 |
| 0.77 | 0.78 | -0.02 | -0.03 |
| 4.55 | 5.05 | -0.10 | -0.19 |
| 0.00 | 2.92 | 0.00 | 0.00 |
| 1.93 | 2.04 | -0.06 | -0.10 |
| 2.77 | 3.50 | -0.23 | -0.42 |
| 0.00 | 0.19 | 0.00 | 0.00 |
| 3.47 | 3.94 | -0.13 | -0.23 |
| 0.92 | 0.76 | 0.19 | 0.34 |
| 0.00 | 0.74 | 0.00 | 0.00 |
| 0.00 | 1.99 | 0.00 | 0.00 |
| 0.00 | 1.29 | 0.00 | 0.00 |
| 1.21 | 1.07 | 0.12 | 0.22 |
| 6.90 | 6.91 | -0.00 | -0.00 |
| 0.00 | 4.00 | 0.00 | 0.00 |
| 2.45 | 2.80 | -0.13 | -0.24 |
| 0.00 | 4.79 | 0.00 | 0.00 |
| 0.00 | 0.26 | 0.00 | 0.00 |
| 4.52 | 5.40 | -0.18 | -0.32 |

TABLE 9. (CONT.)

| ORIG. RATE | FITTED RATE | RESIDUAL | STAND. RES. |
|------------|-------------|----------|-------------|
| 0.00 | 0.31 | 0.00 | 0.00 |
| 0.00 | 1.98 | 0.00 | 0.00 |
| 0.00 | 1.15 | 0.00 | 0.00 |
| 0.00 | 0.80 | 0.00 | 0.00 |
| 0.00 | 1.37 | 0.00 | 0.00 |
| 0.00 | 0.08 | 0.00 | 0.00 |
| 0.00 | 1.55 | 0.00 | 0.00 |
| 0.00 | 0.39 | 0.00 | 0.00 |
| 0.00 | 0.38 | 0.00 | 0.00 |
| 0.73 | 1.02 | -0.34 | -0.61 |
| 0.00 | 0.66 | 0.00 | 0.00 |
| 0.00 | 0.55 | 0.00 | 0.00 |
| 3.22 | 3.56 | -0.10 | -0.18 |
| 0.00 | 2.06 | 0.00 | 0.00 |
| 2.24 | 1.44 | 0.44 | 0.80 |
| 0.00 | 2.47 | 0.00 | 0.00 |
| 0.00 | 0.14 | 0.00 | 0.00 |
| 0.00 | 2.78 | 0.00 | 0.00 |
| 1.00 | 0.86 | 0.15 | 0.27 |
| 0.00 | 0.83 | 0.00 | 0.00 |
| 0.82 | 2.24 | -1.01 | -1.82 |
| 3.11 | 1.45 | 0.76 | 1.37 |
| 0.00 | 1.21 | 0.00 | 0.00 |
| 8.53 | 7.81 | 0.09 | 0.16 |
| 1.35 | 4.52 | -1.21 | -2.18 |
| 4.87 | 3.16 | 0.43 | 0.78 |
| 11.68 | 5.41 | 0.77 | 1.39 |
| 0.30 | 0.30 | 0.01 | 0.02 |
| 0.00 | 6.09 | 0.00 | 0.00 |
| 0.19 | 0.81 | -1.45 | -2.61 |
| 0.00 | 0.78 | 0.00 | 0.00 |
| 1.14 | 2.11 | -0.61 | -1.11 |
| 2.39 | 1.36 | 0.56 | 1.01 |
| 0.00 | 1.14 | 0.00 | 0.00 |
| 13.41 | 7.33 | 0.60 | 1.09 |
| 5.75 | 4.24 | 0.30 | 0.55 |
| 2.06 | 2.97 | -0.36 | -0.66 |
| 13.19 | 5.08 | 0.95 | 1.72 |
| 0.28 | 0.28 | 0.00 | 0.01 |
| 0.00 | 5.72 | 0.00 | 0.00 |
| 0.53 | 0.66 | -0.21 | -0.39 |
| 0.00 | 0.64 | 0.00 | 0.00 |
| 0.00 | 1.71 | 0.00 | 0.00 |
| 0.84 | 1.11 | -0.28 | -0.50 |
| 0.00 | 0.92 | 0.00 | 0.00 |
| 6.33 | 5.96 | 0.06 | 0.11 |
| 2.81 | 3.45 | -0.21 | -0.37 |
| 5.22 | 2.41 | 0.77 | 1.39 |
| 3.90 | 4.13 | -0.06 | -0.10 |
| 0.21 | 0.23 | -0.08 | -0.14 |
| 0.00 | 4.65 | 0.00 | 0.00 |
| 0.10 | 0.43 | -1.47 | -2.65 |
| 0.00 | 0.42 | 0.00 | 0.00 |
| 0.00 | 1.13 | 0.00 | 0.00 |
| 0.78 | 0.73 | 0.06 | 0.11 |
| 0.00 | 0.61 | 0.00 | 0.00 |
| 4.18 | 3.95 | 0.06 | 0.10 |
| 4.73 | 2.29 | 0.73 | 1.31 |
| 0.00 | 1.60 | 0.00 | 0.00 |
| 4.80 | 2.74 | 0.56 | 1.02 |
| 0.16 | 0.15 | 0.06 | 0.11 |

TABLE 9. (CONT.)

| ORIG. RATE | FITTED RATE | RESIDUAL | STAND. RES. |
|------------|-------------|----------|-------------|
| 0.83 | 0.80 | 0.03 | 0.06 |
| 0.00 | 0.78 | 0.00 | 0.00 |
| 0.00 | 2.10 | 0.00 | 0.00 |
| 0.00 | 1.36 | 0.00 | 0.00 |
| 0.00 | 1.13 | 0.00 | 0.00 |
| 12.33 | 7.30 | 0.52 | 0.95 |
| 0.00 | 4.22 | 0.00 | 0.00 |
| 1.69 | 2.95 | -0.56 | -1.01 |
| 0.00 | 5.06 | 0.00 | 0.00 |
| 0.00 | 0.28 | 0.00 | 0.00 |
| 5.70 | 5.70 | 0.00 | 0.00 |
| 1.21 | 1.08 | 0.11 | 0.20 |
| 0.00 | 1.05 | 0.00 | 0.00 |
| 0.00 | 2.83 | 0.00 | 0.00 |
| 0.00 | 1.83 | 0.00 | 0.00 |
| 1.80 | 1.52 | 0.17 | 0.30 |
| 5.14 | 9.84 | -0.65 | -1.17 |
| 8.57 | 5.70 | 0.41 | 0.74 |
| 3.84 | 3.98 | -0.04 | -0.06 |
| 0.00 | 6.82 | 0.00 | 0.00 |
| 0.00 | 0.37 | 0.00 | 0.00 |
| 0.00 | 7.68 | 0.00 | 0.00 |
| 1.00 | 0.83 | 0.24 | 0.43 |
| 0.00 | 0.81 | 0.00 | 0.00 |
| 0.00 | 2.18 | 0.00 | 0.00 |
| 0.00 | 1.41 | 0.00 | 0.00 |
| 1.28 | 1.17 | 0.09 | 0.16 |
| 7.11 | 7.57 | -0.06 | -0.11 |
| 6.25 | 4.38 | 0.35 | 0.64 |
| 1.65 | 3.06 | -0.62 | -1.12 |
| 0.00 | 5.25 | 0.00 | 0.00 |
| 0.00 | 0.29 | 0.00 | 0.00 |
| 0.00 | 5.91 | 0.00 | 0.00 |
| 2.15 | 1.41 | 0.42 | 0.76 |
| 0.00 | 1.37 | 0.00 | 0.00 |
| 0.00 | 3.69 | 0.00 | 0.00 |
| 0.00 | 2.39 | 0.00 | 0.00 |
| 2.10 | 1.99 | 0.06 | 0.10 |
| 15.56 | 12.83 | 0.19 | 0.35 |
| 9.18 | 7.43 | 0.21 | 0.38 |
| 2.15 | 5.19 | -0.88 | -1.59 |
| 0.00 | 8.89 | 0.00 | 0.00 |
| 0.00 | 0.49 | 0.00 | 0.00 |
| 0.00 | 10.01 | 0.00 | 0.00 |
| 2.96 | 1.90 | 0.44 | 0.80 |
| 0.00 | 1.85 | 0.00 | 0.00 |
| 0.00 | 4.97 | 0.00 | 0.00 |
| 0.00 | 3.22 | 0.00 | 0.00 |
| 1.52 | 2.68 | -0.57 | -1.02 |
| 15.23 | 17.29 | -0.13 | -0.23 |
| 12.87 | 10.01 | 0.25 | 0.45 |
| 0.00 | 6.99 | 0.00 | 0.00 |
| 0.00 | 11.98 | 0.00 | 0.00 |
| 0.00 | 0.66 | 0.00 | 0.00 |
| 0.00 | 13.49 | 0.00 | 0.00 |
| 1.65 | 1.30 | 0.24 | 0.43 |
| 0.00 | 1.26 | 0.00 | 0.00 |
| 0.00 | 3.39 | 0.00 | 0.00 |
| 0.00 | 2.19 | 0.00 | 0.00 |
| 1.50 | 1.83 | -0.20 | -0.36 |
| 9.23 | 11.79 | -0.24 | -0.44 |

TABLE 9. (CONT.)

| ORIG. RATE | FITTED RATE | RESIDUAL | STAND. RES. |
|------------|-------------|----------|-------------|
| 0.00 | 3.08 | 0.00 | 0.00 |
| 0.57 | 0.56 | 0.02 | 0.04 |
| 1.09 | 0.54 | 0.62 | 1.11 |
| 0.00 | 1.45 | 0.00 | 0.00 |
| 0.00 | 0.94 | 0.00 | 0.00 |
| 0.54 | 0.78 | -0.37 | -0.67 |
| 3.50 | 5.05 | -0.37 | -0.66 |
| 1.58 | 2.92 | -0.62 | -1.11 |
| 3.73 | 2.04 | 0.60 | 1.09 |
| 3.90 | 3.50 | 0.11 | 0.20 |
| 0.00 | 0.19 | 0.00 | 0.00 |
| 0.00 | 3.94 | 0.00 | 0.00 |
| 0.36 | 0.46 | -0.23 | -0.42 |
| 0.38 | 0.44 | -0.15 | -0.27 |
| 0.00 | 1.19 | 0.00 | 0.00 |
| 1.15 | 0.77 | 0.40 | 0.73 |
| 0.60 | 0.64 | -0.07 | -0.12 |
| 4.57 | 4.13 | 0.10 | 0.18 |
| 1.71 | 2.39 | -0.34 | -0.61 |
| 2.22 | 1.67 | 0.28 | 0.51 |
| 0.00 | 2.86 | 0.00 | 0.00 |
| 0.00 | 0.16 | 0.00 | 0.00 |
| 0.00 | 3.23 | 0.00 | 0.00 |
| 0.39 | 0.34 | 0.15 | 0.27 |
| 0.26 | 0.33 | -0.23 | -0.41 |
| 0.00 | 0.88 | 0.00 | 0.00 |
| 0.20 | 0.57 | -1.05 | -1.89 |
| 0.63 | 0.47 | 0.29 | 0.51 |
| 0.00 | 3.06 | 0.00 | 0.00 |
| 0.00 | 1.77 | 0.00 | 0.00 |
| 2.87 | 1.24 | 0.84 | 1.52 |
| 0.00 | 2.12 | 0.00 | 0.00 |
| 0.00 | 0.12 | 0.00 | 0.00 |
| 0.00 | 2.39 | 0.00 | 0.00 |
| 0.48 | 0.49 | -0.02 | -0.03 |
| 0.52 | 0.47 | 0.09 | 0.17 |
| 0.00 | 1.27 | 0.00 | 0.00 |
| 0.47 | 0.82 | -0.56 | -1.01 |
| 1.11 | 0.69 | 0.48 | 0.87 |
| 0.00 | 4.43 | 0.00 | 0.00 |
| 0.00 | 2.56 | 0.00 | 0.00 |
| 0.00 | 1.79 | 0.00 | 0.00 |
| 0.00 | 3.07 | 0.00 | 0.00 |
| 0.00 | 0.17 | 0.00 | 0.00 |
| 0.00 | 3.46 | 0.00 | 0.00 |
| 0.54 | 0.52 | 0.04 | 0.08 |
| 0.36 | 0.50 | -0.33 | -0.60 |
| 0.00 | 1.35 | 0.00 | 0.00 |
| 1.17 | 0.87 | 0.29 | 0.53 |
| 0.00 | 0.73 | 0.00 | 0.00 |
| 0.00 | 4.70 | 0.00 | 0.00 |
| 0.00 | 2.72 | 0.00 | 0.00 |
| 0.00 | 1.90 | 0.00 | 0.00 |
| 0.00 | 3.26 | 0.00 | 0.00 |
| 0.00 | 0.18 | 0.00 | 0.00 |
| 0.00 | 3.67 | 0.00 | 0.00 |
| 0.58 | 0.80 | -0.32 | -0.58 |
| 0.00 | 0.78 | 0.00 | 0.00 |
| 3.50 | 2.09 | 0.51 | 0.93 |
| 1.12 | 1.35 | -0.19 | -0.34 |
| 0.00 | 1.13 | 0.00 | 0.00 |

TABLE 9. (CONT.)

| ORIG. RATE | FITTED RATE | RESIDUAL | STAND. RES. |
|------------|-------------|----------|-------------|
| 7.17 | 6.82 | 0.05 | 0.09 |
| 5.55 | 4.77 | 0.15 | 0.27 |
| 0.00 | 8.17 | 0.00 | 0.00 |
| 0.00 | 0.45 | 0.00 | 0.00 |
| 0.00 | 9.20 | 0.00 | 0.00 |
| 0.81 | 1.01 | -0.22 | -0.40 |
| 0.00 | 0.98 | 0.00 | 0.00 |
| 0.00 | 2.64 | 0.00 | 0.00 |
| 0.00 | 1.71 | 0.00 | 0.00 |
| 0.00 | 1.42 | 0.00 | 0.00 |
| 10.80 | 9.18 | 0.16 | 0.29 |
| 5.63 | 5.31 | 0.06 | 0.11 |
| 0.00 | 3.71 | 0.00 | 0.00 |
| 0.00 | 6.36 | 0.00 | 0.00 |
| 0.00 | 0.35 | 0.00 | 0.00 |
| 0.00 | 7.16 | 0.00 | 0.00 |
| 0.00 | 0.83 | 0.00 | 0.00 |
| 0.00 | 0.80 | 0.00 | 0.00 |
| 0.00 | 2.16 | 0.00 | 0.00 |
| 0.00 | 1.40 | 0.00 | 0.00 |
| 0.00 | 1.17 | 0.00 | 0.00 |
| 0.00 | 7.53 | 0.00 | 0.00 |
| 4.36 | 4.36 | 0.00 | 0.00 |
| 0.00 | 3.05 | 0.00 | 0.00 |
| 0.00 | 5.22 | 0.00 | 0.00 |
| 0.00 | 0.29 | 0.00 | 0.00 |
| 0.00 | 5.88 | 0.00 | 0.00 |

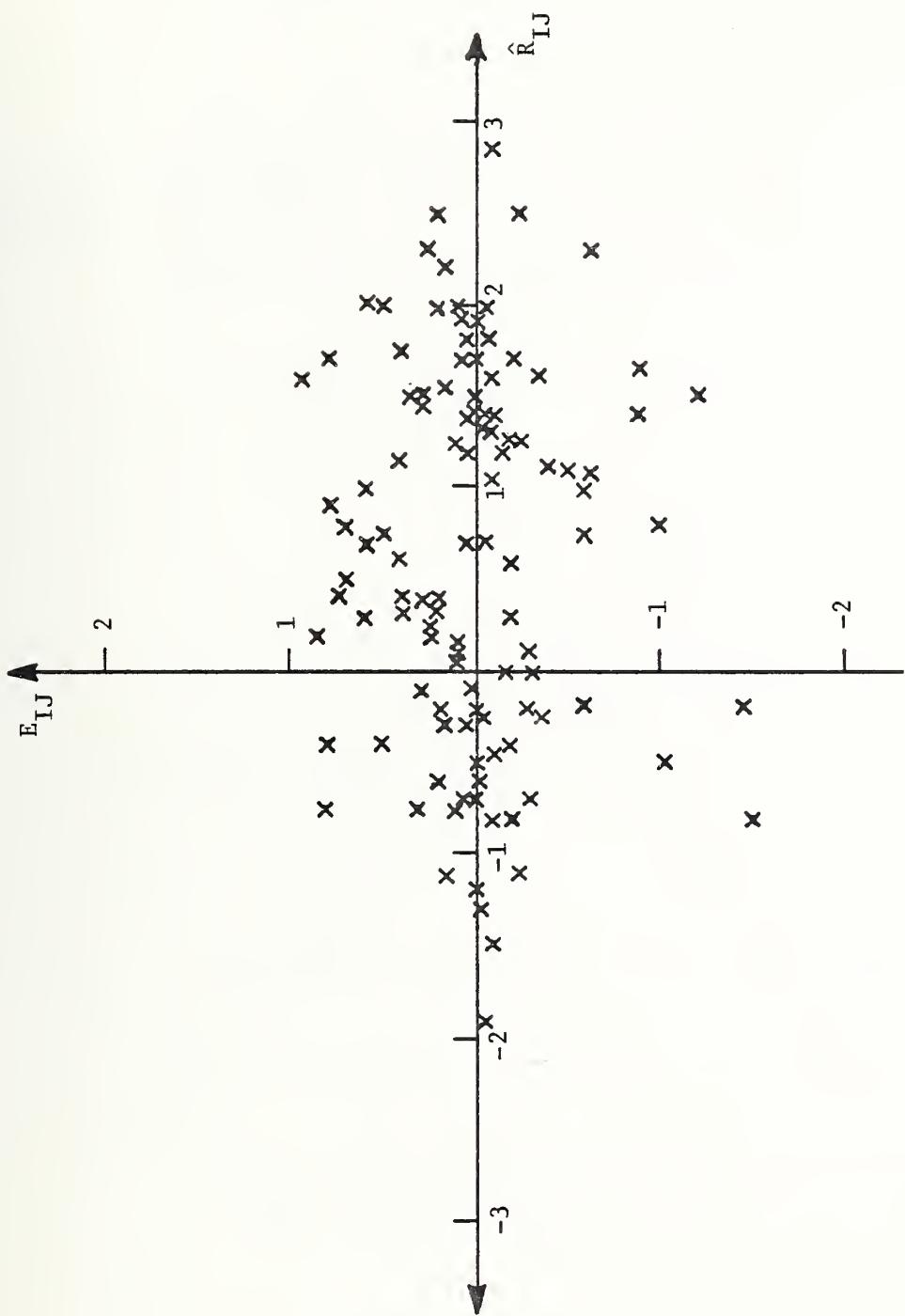


FIGURE 11. PLOT OF THE RESIDUALS, E_{IJ} , VS. THE PREDICTED VALUES, \hat{R}_{IJ}
(TRANSFORMED DATA)

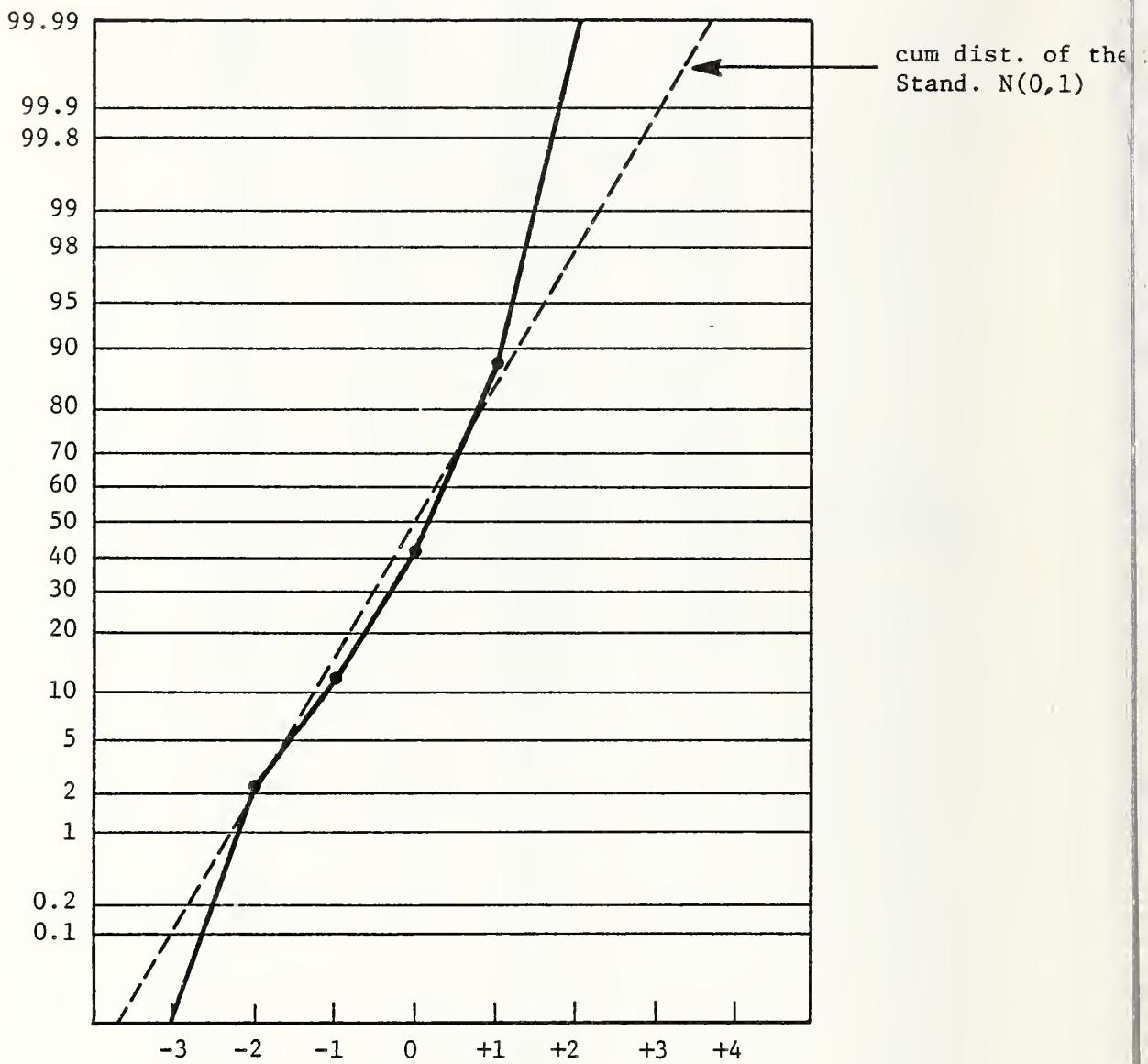


FIGURE 12. NORMALITY PLOT OF THE STANDARDIZED RESIDUALS, E_{IJ} (TRANSFORMED DATA)

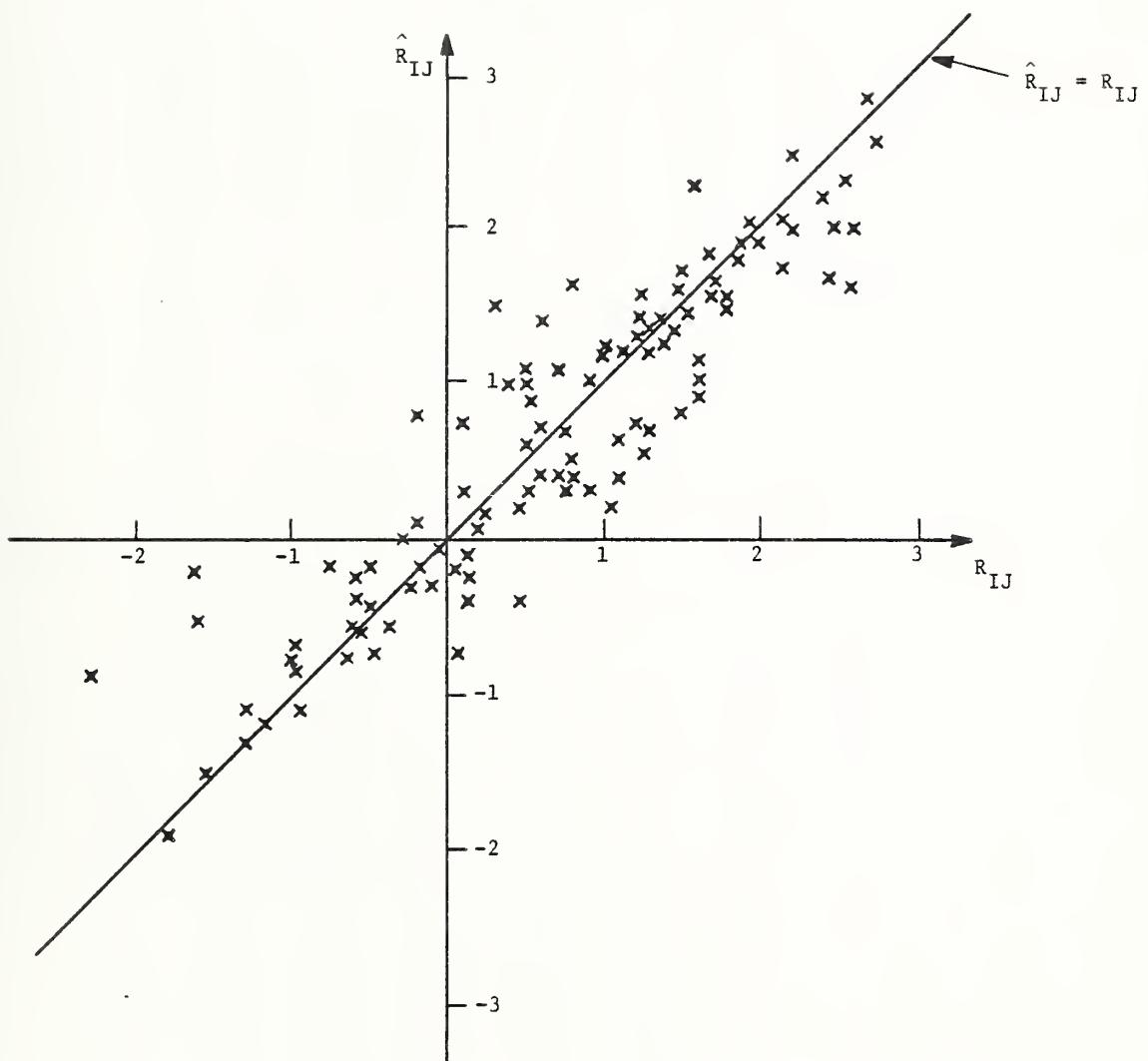


FIGURE 13. PLOT OF THE PREDICTED VALUES, \hat{R}_{IJ} , VS. THE ACTUAL, R_{IJ}

on, assumptions such as constant variance and normality of the residuals. Note also that the estimated values are positive throughout while Model (2) produces negative estimates occasionally. At this point, Model (3) is accepted as a reasonably good model for our purposes, and is applied to the other three matrices in Tables 5 through 7. The results are presented in Appendix 13. Tables 10 through 13 present the final matrices with all the empty cells filled with the estimated values derived using Model (3).

VI. Evaluation of Survey Results

Model (3) gives an estimated time series, \hat{R}_{IJ} of passenger rate of flow at the underground stations. It postulates that the expected value of each of these estimated volumes is a multiplicative function of "station" and "time" effects. Hence the variance of these estimates is again a function of the variances and covariances of these estimated effects a_I , or b_J , etc. Since the regression is performed on the transformed data, it is necessary to re-express variances and expected values to their original forms for more meaningful interpretation. Essentially, Model (3) has:

$$\log \hat{R}_{IJ} = \hat{u} + \hat{a}_I + \hat{b}_J$$

$$\begin{aligned} \text{var}(\log \hat{R}_{IJ}) &= V(\hat{u}) + V(\hat{a}_I) + V(\hat{b}_J) + 2 \text{Cov}(\hat{u}, \hat{a}_I) \\ &\quad + 2 \text{Cov}(\hat{a}_I, \hat{b}_J) + 2 \text{Cov}(\hat{u}, \hat{b}_J) \end{aligned}$$

TABLE 10. ESTIMATED LOADING RATE (ALL RIVERSIDE TRAINS)

| TIME | KEN. | AUD. | COP. | ARL. | BOYL. | PARK | GOV. | HAY. | N. | SCI. | LECM. |
|------|------|------|------|------|-------|-------|-------|------|-------|------|-------|
| | | | | | | | CTR. | | STA. | PK. | |
| 700 | 0.22 | 0.21 | 0.57 | 0.37 | 0.31 | 1.98 | 1.15 | 0.80 | 1.37 | 0.08 | 1.55 |
| 730 | 0.39 | 0.38 | 1.02 | 0.66 | 0.55 | 3.56 | 2.06 | 1.44 | 2.47 | 0.14 | 2.78 |
| 800 | 0.86 | 0.83 | 2.24 | 1.45 | 1.21 | 7.81 | 4.52 | 3.16 | 5.41 | 0.30 | 6.09 |
| 830 | 0.81 | 0.78 | 2.11 | 1.36 | 1.14 | 7.33 | 4.24 | 2.97 | 5.08 | 0.28 | 5.72 |
| 900 | 0.66 | 0.64 | 1.71 | 1.11 | 0.92 | 5.96 | 3.45 | 2.41 | 4.13 | 0.23 | 4.65 |
| 930 | 0.43 | 0.42 | 1.13 | 0.73 | 0.61 | 3.95 | 2.29 | 1.60 | 2.74 | 0.15 | 3.08 |
| 1000 | 0.56 | 0.54 | 1.45 | 0.94 | 0.78 | 5.05 | 2.92 | 2.04 | 3.50 | 0.19 | 3.94 |
| 1030 | 0.46 | 0.44 | 1.19 | 0.77 | 0.64 | 4.13 | 2.39 | 1.67 | 2.86 | 0.16 | 3.23 |
| 1100 | 0.34 | 0.33 | 0.88 | 0.57 | 0.47 | 3.06 | 1.77 | 1.24 | 2.12 | 0.12 | 2.39 |
| 1130 | 0.49 | 0.47 | 1.27 | 0.82 | 0.69 | 4.43 | 2.56 | 1.79 | 3.07 | 0.17 | 3.46 |
| 1200 | 0.52 | 0.50 | 1.35 | 0.87 | 0.73 | 4.70 | 2.72 | 1.90 | 3.26 | 0.18 | 3.67 |
| 1230 | 0.80 | 0.78 | 2.09 | 1.35 | 1.13 | 7.28 | 4.22 | 2.94 | 5.04 | 0.28 | 5.68 |
| 1300 | 0.54 | 0.53 | 1.42 | 0.92 | 0.76 | 4.93 | 2.86 | 1.99 | 3.42 | 0.19 | 3.85 |
| 1330 | 0.47 | 0.46 | 1.24 | 0.80 | 0.67 | 4.31 | 2.49 | 1.74 | 2.99 | 0.16 | 3.36 |
| 1400 | 0.66 | 0.64 | 1.72 | 1.11 | 0.92 | 5.97 | 3.46 | 2.41 | 4.14 | 0.23 | 4.66 |
| 1430 | 0.56 | 0.54 | 1.45 | 0.94 | 0.78 | 5.05 | 2.92 | 2.04 | 3.50 | 0.19 | 3.94 |
| 1500 | 0.76 | 0.74 | 1.99 | 1.29 | 1.07 | 6.91 | 4.00 | 2.80 | 4.79 | 0.26 | 5.40 |
| 1530 | 0.80 | 0.78 | 2.10 | 1.36 | 1.13 | 7.30 | 4.22 | 2.95 | 5.06 | 0.28 | 5.70 |
| 1600 | 1.08 | 1.05 | 2.83 | 1.83 | 1.52 | 9.84 | 5.70 | 3.98 | 6.82 | 0.37 | 7.68 |
| 1630 | 0.83 | 0.81 | 2.18 | 1.41 | 1.17 | 7.57 | 4.38 | 3.06 | 5.25 | 0.29 | 5.91 |
| 1700 | 1.41 | 1.37 | 3.69 | 2.39 | 1.99 | 12.83 | 7.43 | 5.19 | 8.89 | 0.49 | 10.01 |
| 1730 | 1.90 | 1.85 | 4.97 | 3.22 | 2.68 | 17.29 | 10.01 | 6.99 | 11.98 | 0.66 | 13.49 |
| 1800 | 1.30 | 1.26 | 3.39 | 2.19 | 1.83 | 11.79 | 6.82 | 4.77 | 8.17 | 0.45 | 9.20 |
| 1830 | 1.01 | 0.98 | 2.64 | 1.71 | 1.42 | 9.18 | 5.31 | 3.71 | 6.36 | 0.35 | 7.16 |
| 1900 | 0.83 | 0.80 | 2.16 | 1.40 | 1.17 | 7.83 | 4.36 | 3.05 | 5.22 | 0.29 | 5.88 |

TABLE 11. ESTIMATED UNLOADING RATES (ALL RIVERSIDE TRAINS)

| TIME | KEN. | AUD. | COP. | ARL. | BOYL. | PARK | GOV. | HAY. |
|------|-------|------|-------|------|-------|------|------|------|
| | | | | | | | CTR. | |
| 700 | 2.48 | 1.20 | 4.57 | 2.82 | 0.50 | 2.49 | 0.52 | 0.06 |
| 730 | 1.38 | 0.66 | 3.16 | 1.56 | 0.28 | 1.22 | 0.29 | 0.04 |
| 800 | 3.00 | 1.72 | 6.68 | 8.20 | 0.71 | 1.97 | 1.00 | 0.09 |
| 830 | 4.19 | 2.27 | 8.19 | 7.91 | 0.94 | 4.74 | 1.96 | 0.06 |
| 900 | 5.05 | 1.77 | 6.77 | 4.26 | 0.74 | 3.20 | 0.57 | 0.13 |
| 930 | 1.79 | 0.91 | 3.47 | 2.17 | 0.38 | 1.76 | 0.44 | 0.06 |
| 1000 | 1.33 | 4.33 | 6.64 | 4.09 | 0.81 | 3.25 | 0.81 | 0.12 |
| 1030 | 1.44 | 0.66 | 3.87 | 2.65 | 1.65 | 1.17 | 0.43 | 0.07 |
| 1100 | 1.78 | 0.35 | 1.64 | 0.55 | 0.20 | 0.89 | 0.19 | 0.03 |
| 1130 | 1.55 | 0.71 | 3.01 | 0.80 | 0.89 | 1.64 | 0.34 | 0.05 |
| 1200 | 1.68 | 0.73 | 3.33 | 2.63 | 0.36 | 1.81 | 0.38 | 0.06 |
| 1230 | 0.48 | 0.59 | 6.00 | 1.35 | 0.25 | 1.23 | 0.26 | 0.04 |
| 1300 | 1.64 | 0.79 | 3.03 | 1.87 | 0.33 | 1.65 | 0.34 | 0.05 |
| 1330 | 1.77 | 0.79 | 2.80 | 1.86 | 0.33 | 1.65 | 0.34 | 0.05 |
| 1400 | 2.32 | 1.43 | 3.15 | 3.36 | 0.44 | 3.48 | 0.62 | 0.24 |
| 1430 | 6.42 | 0.98 | 2.20 | 2.30 | 0.18 | 2.28 | 0.42 | 0.07 |
| 1500 | 3.81 | 0.88 | 3.38 | 2.08 | 0.34 | 1.87 | 0.38 | 0.03 |
| 1530 | 1.87 | 1.70 | 6.50 | 4.01 | 0.20 | 7.00 | 0.74 | 0.38 |
| 1600 | 2.66 | 2.04 | 7.78 | 4.80 | 2.60 | 3.38 | 0.57 | 0.14 |
| 1630 | 3.38 | 2.47 | 9.44 | 5.82 | 1.09 | 4.31 | 1.82 | 0.16 |
| 1700 | 7.38 | 2.34 | 8.95 | 5.52 | 1.34 | 8.76 | 1.05 | 0.04 |
| 1730 | 10.04 | 1.82 | 6.94 | 4.28 | 0.18 | 5.37 | 0.87 | 0.12 |
| 1800 | 8.06 | 2.84 | 10.86 | 6.69 | 0.94 | 4.00 | 0.63 | 0.50 |
| 1830 | 2.75 | 1.55 | 5.91 | 3.64 | 0.64 | 5.70 | 0.44 | 0.10 |
| 1900 | 0.34 | 0.16 | 0.62 | 0.38 | 0.07 | 0.34 | 0.07 | 0.01 |

TABLE 12. ESTIMATED LOADING RATES
(ALL NORTH STATION TRAINS)

| TIME | KEN. | AUD. | COP. | ARL. | BOYL. | PARK | GOV. | HAY. |
|------|------|------|------|------|-------|------|------|------|
| | | | | | | | CTR. | |
| 700 | 0.32 | 0.23 | 0.33 | 0.19 | 0.04 | 0.23 | 0.05 | 0.02 |
| 730 | 0.45 | 0.33 | 0.47 | 0.27 | 0.06 | 0.33 | 0.07 | 0.03 |
| 800 | 2.63 | 1.94 | 1.75 | 1.56 | 0.36 | 8.10 | 0.14 | 0.17 |
| 830 | 3.06 | 1.80 | 3.36 | 1.84 | 0.33 | 2.28 | 0.13 | 0.16 |
| 900 | 5.81 | 2.01 | 2.82 | 2.17 | 0.37 | 0.63 | 0.43 | 0.18 |
| 930 | 1.14 | 1.08 | 1.51 | 0.42 | 0.20 | 0.79 | 0.54 | 0.13 |
| 1000 | 0.35 | 0.96 | 1.18 | 0.68 | 0.33 | 1.21 | 0.15 | 0.07 |
| 1030 | 1.14 | 1.66 | 1.34 | 0.92 | 0.07 | 1.00 | 0.33 | 0.06 |
| 1100 | 3.29 | 1.13 | 0.94 | 1.00 | 0.16 | 0.81 | 0.94 | 0.12 |
| 1130 | 0.93 | 1.45 | 1.26 | 0.36 | 0.62 | 0.95 | 0.11 | 0.08 |
| 1200 | 1.75 | 0.62 | 0.46 | 0.56 | 0.11 | 0.62 | 0.10 | 0.05 |
| 1230 | 1.66 | 0.89 | 5.23 | 0.71 | 0.16 | 0.88 | 0.03 | 0.08 |
| 1300 | 1.11 | 0.82 | 1.15 | 0.66 | 0.15 | 0.81 | 0.16 | 0.07 |
| 1330 | 2.94 | 1.25 | 1.60 | 1.01 | 0.23 | 1.24 | 0.24 | 0.07 |
| 1400 | 3.84 | 1.30 | 2.38 | 1.04 | 0.24 | 1.29 | 0.25 | 0.04 |
| 1430 | 3.96 | 1.27 | 1.74 | 1.02 | 0.23 | 1.26 | 0.25 | 0.05 |
| 1500 | 3.00 | 2.21 | 3.11 | 1.78 | 0.41 | 2.19 | 0.43 | 0.19 |
| 1530 | 6.84 | 5.05 | 7.10 | 4.05 | 0.93 | 5.00 | 0.98 | 0.44 |
| 1600 | 2.00 | 2.62 | 3.68 | 2.10 | 0.48 | 1.80 | 1.30 | 0.23 |
| 1630 | 3.67 | 2.54 | 4.54 | 2.59 | 0.63 | 5.81 | 0.24 | 0.58 |
| 1700 | 2.14 | 1.36 | 4.93 | 1.58 | 1.09 | 2.18 | 0.90 | 2.22 |
| 1730 | 4.35 | 4.90 | 5.67 | 3.90 | 0.53 | 5.70 | 0.97 | 0.24 |
| 1800 | 1.08 | 1.42 | 1.88 | 2.50 | 0.08 | 1.00 | 0.72 | 0.12 |
| 1830 | 0.83 | 1.13 | 1.59 | 1.19 | 0.25 | 1.11 | 0.26 | 0.10 |

TABLE 13. ESTIMATED UNLOADING RATES
(ALL NORTH STATION TRAINS)

| TIME | KEN. | AUD. | COP. | ARL. | BOYL. | PARK | GOV. | HAY. | N. STA. |
|------|------|------|------|------|-------|-------|-------|------|------------|
| | | | | | | | CTR. | | |
| 700 | 0.19 | 0.47 | 0.47 | 0.57 | 0.25 | 3.30 | 2.04 | 0.84 | 0.67 |
| 730 | 0.39 | 0.96 | 0.95 | 1.15 | 0.51 | 6.68 | 4.12 | 1.69 | 1.36 |
| 800 | 1.42 | 3.49 | 2.69 | 4.18 | 1.85 | 22.07 | 20.43 | 6.16 | 5.15 |
| 830 | 0.50 | 1.93 | 3.96 | 3.90 | 1.02 | 10.69 | 11.65 | 3.40 | 1.09 |
| 900 | 0.38 | 2.32 | 2.30 | 4.67 | 1.23 | 13.07 | 16.97 | 4.09 | 3.53 |
| 930 | 0.59 | 1.00 | 0.99 | 2.96 | 0.53 | 5.56 | 7.15 | 0.47 | 1.09 |
| 1000 | 0.35 | 2.67 | 1.25 | 1.51 | 0.89 | 8.66 | 6.88 | 0.94 | 1.80 |
| 1030 | 0.47 | 1.45 | 1.02 | 1.46 | 0.52 | 5.11 | 2.93 | 2.22 | 1.47 |
| 1100 | 0.43 | 1.45 | 1.44 | 1.57 | 0.61 | 7.19 | 3.97 | 0.49 | 1.40 |
| 1130 | 0.29 | 0.68 | 0.85 | 0.62 | 1.12 | 4.88 | 1.14 | 1.24 | 1.00 |
| 1200 | 0.32 | 0.97 | 1.19 | 0.96 | 0.52 | 6.78 | 5.10 | 1.72 | 1.38 |
| 1230 | 0.88 | 1.42 | 1.15 | 1.70 | 0.75 | 9.90 | 4.92 | 2.51 | 2.02 |
| 1300 | 0.33 | 1.43 | 1.41 | 1.71 | 0.76 | 9.92 | 6.12 | 2.51 | 3.56 |
| 1330 | 0.59 | 0.78 | 0.68 | 0.93 | 0.41 | 5.39 | 3.33 | 0.50 | 2.14 |
| 1400 | 1.09 | 1.75 | 2.00 | 2.10 | 0.93 | 12.19 | 7.52 | 2.39 | 1.82 |
| 1430 | 1.04 | 1.41 | 0.72 | 1.69 | 0.75 | 9.82 | 6.06 | 2.26 | 2.36 |
| 1500 | 0.55 | 1.35 | 0.80 | 1.61 | 0.71 | 9.38 | 5.79 | 3.69 | 1.92 |
| 1530 | 0.60 | 1.48 | 1.47 | 1.78 | 0.79 | 10.33 | 6.37 | 2.62 | 2.11 |
| 1600 | 0.29 | 1.02 | 1.01 | 1.23 | 0.54 | 8.17 | 5.52 | 1.81 | 1.46 |
| 1630 | 0.39 | 0.85 | 1.21 | 1.47 | 0.38 | 16.22 | 4.79 | 3.96 | 1.74 |
| 1700 | 0.23 | 0.71 | 1.09 | 0.50 | 0.74 | 10.30 | 4.67 | 9.04 | 1.56 |
| 1730 | 0.39 | 0.90 | 1.28 | 0.94 | 0.41 | 12.33 | 5.34 | 9.05 | 1.83 |
| 1800 | 0.50 | 0.77 | 1.00 | 0.88 | 0.46 | 7.70 | 3.62 | 3.41 | 1.44 |
| 1830 | 1.37 | 0.80 | 0.79 | 0.85 | 0.25 | 3.66 | 2.39 | 1.41 | 1.14 |

where $\text{Var}(\log \hat{R}_{IJ})$ represents the variance of the present estimate $\log \hat{R}_{IJ}$ from the true mean. Since an actual observed rate of flow varies from the true mean value with variance σ^2 , a predicted value of any individual observation will have variance $(\sigma^2 + \text{Var}(\log \hat{R}_{IJ}))$. To re-express the transformed data to their original form,

$$\hat{R}_{IJ} = e^{\log \hat{R}_{IJ}}$$

$$\text{Var}(\hat{R}_{IJ}) = (\hat{R}_{IJ})^2 \text{Var}(\log \hat{R}_{IJ})$$

and the variance of a predicted individual observation is $(\hat{R}_{IJ})^2 (\sigma^2 + \text{Var}(\log \hat{R}_{IJ}))$. Such is also the variance of the distribution of passenger flow to be calibrated into the simulation model to generate new time series. We choose Park Street Station to illustrate. Figure 14 represents three time series, namely the actual collected data, the estimated data derived from Model (3), and the 95% confidence bound not on the estimated series but rather on a future predicted observation. That is, model (3) gives only an estimated average rate of flow, when given the "station" and "time" are fixed, but in 95 cases out of 100, an individual observation will fall within the confidence bound. The wide confidence band indicates that any actual observed series of passenger flow data is expected to behave rather sporadically around the means.

VII. Conclusion

In improving the operational performance of the Light Rail Vehicles in terms of maximizing the utility of the LRV

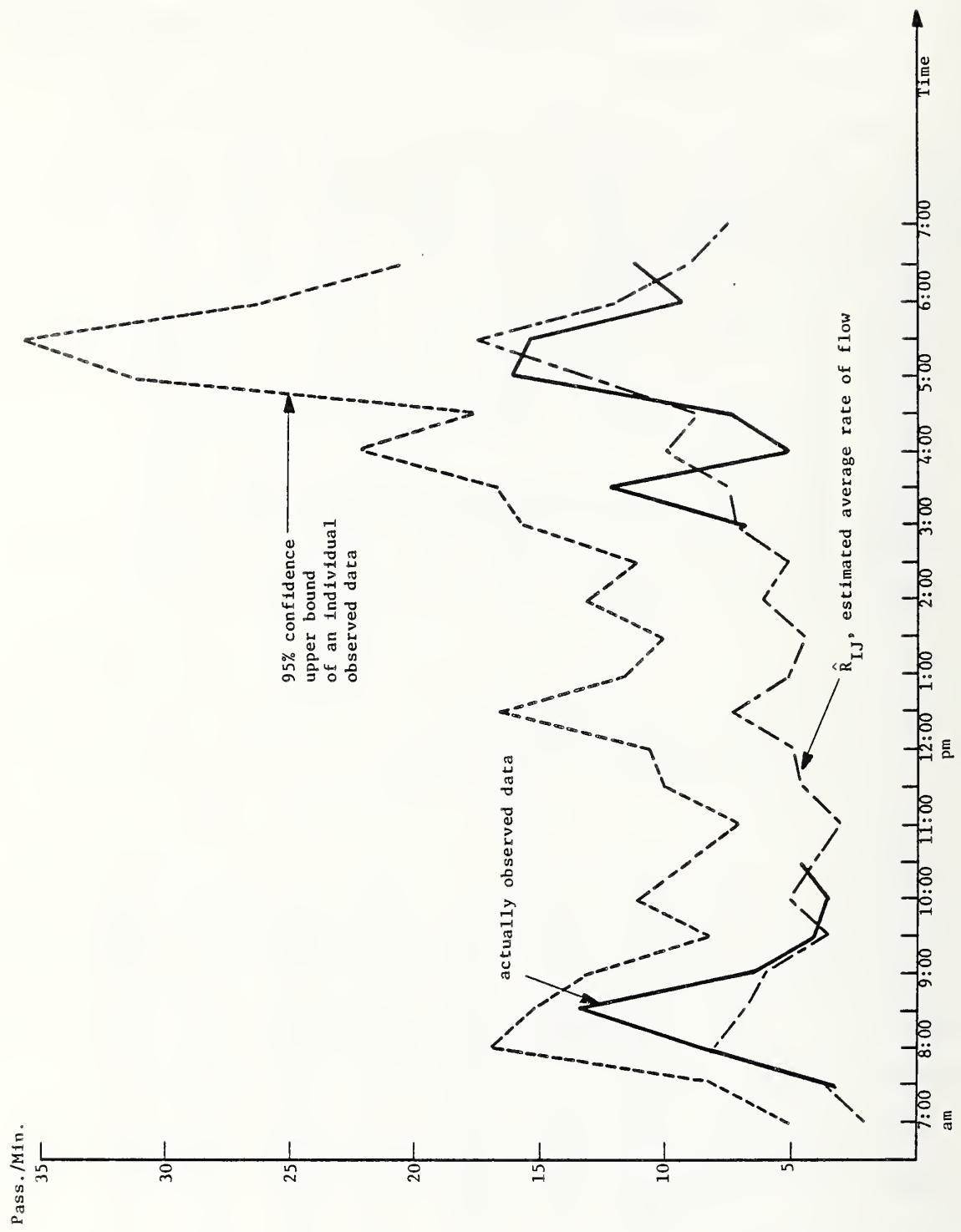


FIGURE 14. PROFILE OF LOADING PASSENGERS AT PARK STREET STATION, 1978
(TO RIVERSIDE)

cars and reducing passengers' waiting time, information about the present distribution of ridership of a transit line is essential. This study has shown that sufficiently accurate and quantitative knowledge about such distributions at different stations can be gained without expending huge amounts of labor and financial resources. Through the use of sampling techniques, from sampling days/shifts and stations to sampling cars or doors of cars, and through the application of a simple statistical model in which "station" and "time" are the determining factors, a representative daily ridership profile for each station has been obtained. However, there is still room for improvement. For example, the problem of sample size has not been addressed. Had a replicated sampling scheme been followed, that is, if for each station-time period combination, more than one observation of the passenger rate of flow were taken, it would be possible to estimate the magnitude of the interaction effect and the pure random error, σ^2 , separately. Also, a cursory look at Table 11, the estimated unloading passenger rate for the Riverside Train reveals abnormally high estimates for Copley during the afternoon rush hours. The environment (mostly business establishments) around the locality does not command such high return rates of passengers.

Validation plans are underway to verify or modify our current estimates. Additional data for the 12:00 - 1:30 period needs to be gathered. However, instead of sampling all stations, it is proposed that only three to four stations

should be observed, and a continuous time series of passenger data be collected. We also need to examine which station and time period in which interaction plays an important part. Also, it is discovered from the data sheets that some surveyors often do not systematically sample the cars when counting passengers from all cars becomes unmanageable. This should be emphasized to assure the representativeness of the collected data, since the distribution of people loading in and out of the two cars is often not uniform. Depending on their proximity to the subway entrance, one car usually gets more passengers than another.

Finally, a word should be said about the estimated total volume of passengers. An earlier study on surface stations has estimated that the daily total number of patrons from the surface section of the Riverside line trains is only approximately 6,800.¹ It would be interesting to see if the data one year later (underground stations) in this study corroborates previous findings. We approximate the total daily volume of passengers going outbound to beyond Kenmore as:

$$\text{Total RIVON outbound} = 30 \left(\sum_{I,J} \hat{R}_{IJ}^{\text{RIVON}} - \sum_{I,J} \hat{R}_{IJ}^{\text{RIVOFF}} \right).$$

¹Kwok, Betty, "MBTA Passenger Demand Analyses, 1977," U.S. Department of Transportation, Urban Mass Transportation Administration, UMTA-MA-06-0074-81-2, August 1981.

This is equivalent to multiplying the "net on" rates (passenger/min.) by 30 (minutes). Similarly, the total number of passengers from the surface stations going inbound to the tunnels is approximated as:

$$\text{TOTAL RIVON inbound} = 30 \left(\sum_{I,J} \hat{R}_{IJ}^{\text{NOROFF}} - \sum_{I,J} \hat{R}_{IJ}^{\text{NORON}} \right).$$

These two statistics are 9,700 and 10,000 respectively. Has the ridership really increased 40%? Statistical variations around earlier estimates and current estimates prohibit such a straightforward conclusion. We can only be contented by the apparent correspondence between the total outbound and inbound volumes, which adds to the credibility and reliability of our passenger flow estimates.

APPENDIX 1
SURVEYOR DATA

DATE 7-5-78

Initial of Observer AA

STATION JOHN LEWIS

Remarks:

Lechmere → Riverside
 Riverside → Lechmere

indicate if count is not for entire train
1. car number - C1, C2, C3
2. door number - D1, D2, D3

indicate any unusual circumstance such as
big groups, etc.

| Time of Arrival | LINE | Car Length | PCC LRV | PASS. ON | PASS. OFF | REMARKS |
|-----------------|------|------------|------------|----------|-----------|---------|
| 7:12 | - | 2 | PCC | 12 | 22 | C1 |
| 7:14 | S | 1 | PCC | | | |
| 7:15 | L | 1 | PCC | 5 | 12 | C1 D1 |
| 7:15 | S | 1 | PCC | | | |
| 7:16 | S | 2 | PCC | 0 | 9 | C1 D1 |
| 7:17 | L | 2 | PCC | 1 | 4 | C1 |
| 7:17 | L | 2 | LRV | 6 | 10 | C1 D1 |
| 7:19 | L | 1 | LRV | 1 | 58 | |
| 7:19 | L | 2 | PCC | 0 | 3 | C1 C2 |
| 7:20 | S | 1 | PCC | | | |
| 7:21 | S | 1 | PCC | | | |
| 7:23 | L | 3 | PCC | 5 | 63 | C-1 |
| 7:24 | L | 2 | PCC | 8 | 25 | C1 |
| 7:25 | N | 2 | LRV | 0 | 11 | C1 D1 |
| 7:26 | GC | 1 | PCC | | | |
| 7:26 | S | 1 | PCC | | | |
| 7:27 | L | 3 | PCC | 24 | 20 | C-1 |
| 7:32 | L | 2 | PCC | 3 | 42 | C-2 |
| 7:33 | GC | 1 | PCC | | | |
| 7:34 | L | 2 | PCC | 6 | 12 | C1 |
| 7:35 | GC | 1 | PCC | | | |
| 7:37 | N | 2 | LRV | 0 | 54 | C2 D1 |
| 7:38 | GC | 2 | LRV | | | |

DATE 5/26/78Initial of Observer LLSTATION GOVERNMENT:

Lechmere → Riverside
 Riverside → Lechmere

Remarks:

indicate if count is not for entire train
 1. car number - C1, C2, C3
 2. door number - D1, D2, D3

indicate any unusual circumstance such as
 big groups, etc.

Last train

| Time of Arrival | LINE | Car Length | PCC LRV | PASS. ON | PASS. OFF | REMARKS |
|-----------------|------|------------|------------|----------|-----------|---------|
| 5:05 | R | 2 | CRV | 58 | 2 | C1 |
| 5:05 | R | 1 | CRV | 35 | 1 | C1 D1 |
| 5:07 | R | 2 | Pu | | | |
| 5:10 | R | 2 | Pu | | | |
| 5:11 | R | 2 | Pu | | | |
| 5:12 | R | 1 | Pu | | | |
| 5:13 | R | 2 | CRV | 11 | 1 | C1 |
| 5:14 | R | 1 | CRV | 11 | 1 | 11 11 |
| 5:16 | R | 2 | Pu | 32 | 2 | C1 |
| 5:17 | R | 2 | - | ... | | -1 |
| 5:22 | R | 1 | Pu | | | |
| 5:23 | R | 2 | Pu | | | |
| 5:24 | R | 2 | Pu | | | |
| 5:27 | R | 1 | Pu | | | |
| 5:28 | R | 2 | Pu | | | |
| 5:29 | R | 2 | Pu | | | |
| 5:30 | R | 2 | CRV | 53 | 5 | C1 |
| 5:35 | R | 1 | Pu | | | |
| 5:36 | R | 2 | Pu | | | |
| 5:37 | R | 1 | Pu | | | |
| 5:37 | R | 2 | CRV | | | |

APPENDIX 2
MBTA FILE STRUCTURE

| | |
|------------|----------------------|
| 780522PARK | 0750H 1PCC |
| 780522PARK | 0751BC1LRV |
| 780522PARK | 0751H 1LRV |
| 780522PARK | 0752H 1PCC |
| 780522PARK | 0753R 2LRV 20 9 X X |
| 780522PARK | 0756CC1LFV |
| 780522PARK | 0757K 2LRV 0 0 |
| 780522PARK | 0757H 1PCC |
| 780522PARK | 0800CC2PCC |
| 780522PARK | 0802R 2LRV 2 4 X X |
| 780522PARK | 0804H 1PCC |
| 780522PARK | 0805CC2PCC |
| 780522PARK | 0805BC3PCC |
| 780522PAFK | 0806H 1LFV |
| 780522PARK | 0809K 1LRV |
| 780522PAFK | 0810BC2PCC |
| 780522PARK | 0812K 2LRV 23 3 X X |
| 780522PARK | 0813CC2PCC |
| 780522PARK | 0815H 1PCC |
| 780522PARK | 0817P 1LRV 22 13 X X |
| 780522PARK | 0815H 1PCC |
| 780522PARK | 0822H 1PCC |
| 780522PAFK | 0824R 2LFV 35 4 X X |
| 780522PARK | 0826H 1PCC |
| 780522PAFK | 0827H 1PCC |
| 780522PAFK | 0831H 1LRV |
| 780522PARK | 0836H 1PCC |
| 780522PARK | 0837BC3PCC |
| 780522PARK | 0838CC2LRV |
| 780522PAFK | 0839CC2PCC |
| 780522PARK | 0840R 2LRV 19 8 X X |
| 780522PARK | 0841CC2PCC |
| 780522PAFK | 0842BC3PCC |
| 780522PAFK | 0842BC3 |
| 780522PAFK | 0843N 1LRV |
| 780522PAFK | 0844H 1PCC |
| 780522PARK | 0844CC2PCC |
| 780522PARK | 0845H 1LFV |
| 780522PARK | 0845CC2PCC |
| 780522PAFK | 0846H 1PCC |
| 780522PARK | 0847R 2LRV 10 11 X X |
| 780522PARK | 0848R 2LRV 5 0 X X |
| 780522PARK | 0849CC2PCC |
| 780522PAFK | 0851H 1PCC |
| 780522PAFK | 0851N 1LFV |
| 780522PAFK | 0854K 2LFV 1 1 |
| 780522PARK | 0854H 1LFV |
| 780522PARK | 0858BC2PCC |
| 780522PAFK | 0859H 1PCC |
| 780522PARK | 0900H 1PCC |
| 780522PARK | 0901CC2PCC |
| 780522PAFK | 0902H 1LRV |
| 780522PAFK | 0902BC3PCC |
| 780522PARK | 0904N 1LRV |
| 780522PAFK | 0904H 1PCC |
| 780522PAFK | 0907K 1LRV |
| 780522PAFK | 0908CC2PCC |
| 780522PARK | 0908BC1LRV |
| 780522PARK | 0909H 2LFV |
| 780522PARK | 0910R 2LRV 13 4 X X |

APPENDIX 3
PROGRAM EXTRAC

```
TYPE EXTRAC
OPEN MBTA.
F STATION EQ "ARLINGTON".
INI 1 ARLING.TON.
SORT BY MAYDAY LINE TIME TYPEOFCAR TRANSIZE.
PRINT ON 1 MAYDAY TIME LINE TRAINSIZE TYPEOFCAR PASSON PASSOFF $
CAR1 CAR2 CAR3 DOOR1 DOOR2 DOOR3 COLLECT FMT D4 I4 A8 I1 A3 &
I3 I3 F1 A1 A1 A1 A1 27 I1 END.
QUIT.
```


APPENDIX 4
PROGRAMS EDIT AND EDIT1

PROGRAM EDIT

```

1      INTEGER LINE, CT, CAR1, CAR2, CAR3, D1, D2, D3
2      CALL IFILE(21, 'REMORE.')
3      CALL OFILE(22, 'STRA1.')
4      IC1D1=0
5      IC1D2=0
6      IC1D3=0
7      IC2D1=0
8      IC2D2=0
9      IC2D3=0
10     IC3D1=0
11     IC3D2=0
12     IC3D3=0
13     READ(21,5,END=100)IDATE,ITIME,LINE,ITS,CT,IUN,IOFF,CAR1,
14     2,CAR2,CAR3,D1,D2,D3,ICOL
15     FORMAT(1B,14,A2,I1,A3,2(I3),6(A1),2X,I1)
16     IF(CT.EQ.'PCC')GO TO 25
17     IF(CAR1.EQ.'X'.AND.CAR2.EQ.'X'.AND.D1.EQ.'X'.
18     2.AND.D3.EQ.'X')GO TO 70
19     IF(CAR1.NE.'X')GO TO 7
20     IF(D1.EQ.'X')IC1D1=1
21     IF(D2.EQ.'X')IC1D2=1
22     IF(D3.EQ.'X')IC1D3=1
23     IF(D1.NE.'X'.AND.D2.NE.'X'.AND.D3.NE.'X')GO TO 6
24     GO TO 7
25     IC1D1=1
26     IC1D2=1
27     IC1D3=1
28     IF(CAR2.NE.'X')GO TO 9
29     IF(D1.EQ.'X')IC2D1=1
30     IF(D2.EQ.'X')IC2D2=1
31     IF(D3.EQ.'X')IC2D3=1
32     IF(D1.NE.'X'.AND.D2.NE.'X'.AND.D3.NE.'X')GO TO 8
33     GO TO 9
34     IC2D1=1
35     IC2D2=1
36     IC2D3=1
37     IF(CAR1.NE.'X'.AND.CAR2.NE.'X'.AND.D1.NE.'X'.
38     2.AND.D2.NE.'X'.AND.D3.NE.'X')GO TO 10
39     GO TO 12
40     IC1D1=1
41     IC1D2=1
42     IC1D3=1
43     IC2D1=1
44     IC2D2=1
45     IC2D3=1
46     IF((IC1D1+IC1D2+IC1D3+IC2D1+IC2D2+IC2D3).GT.0)GO TO 75
47     WRITE(5,14)ITIME, IDATE
48     FORMAT('CANNOT ALLOCATE COUNT TO DDOR AT',1X,I4,
49     2,1X,'UN',1X,I8)
50     GO TO 75
51     IF(CAR1.NE.'X')GO TO 27
52     IF(D1.EQ.'X')IC1D1=1
53     IF(D2.EQ.'X')IC1D2=1
54     IF(D1.NE.'X'.AND.D2.NE.'X')GO TO 26
55     GO TO 27
56     IC1D1=1
57     IC1D2=1
58     IF(CAR2.NE.'X')GO TO 29
59     IF(D1.EQ.'X')IC2D1=1
60     IF(D2.EQ.'X')IC2D2=1
61     IF(D1.NE.'X'.AND.D2.NE.'X')GO TO 28

```

PROGRAM EDIT (CONT.)

```

28      GO TO 29
29      IC2D1=1
      IC2D2=1
      IF(CAR3,NE.,"X")GO TO 31
      IF(I1,EQ.,"X")IC3D1=1
      IF(I2,EQ.,"X")IC3D2=1
      IF(I3,EQ.,"X")AND,I2,NE.,"X")GO TO 30
      GO TO 31
30      IC3D1=1
      IC3D2=1
31      IF(CAR1,NE.,"X",AND,CAR2,NE.,"X",AND,ITS,EQ,2,AND,D1,NE.,"X",
      2 AND,D2,NE.,"X")GO TO 33
      GO TO 34
33      IC1D1=1
      IC1D2=1
      IC2D1=1
      IC2D2=1
34      IF(CAR1,NE.,"X",AND,CAR2,NE.,"X",AND,CAR3,NE.,"X",AND,
      2,ITS,EQ,3,AND,D1,NE.,"X",AND,D2,NE.,"X")GO TO 37
      GO TO 35
35      IC1D1=1
      IC1D2=1
      IC2D1=1
      IC2D2=1
      IC3D1=1
      IC3D2=1
36      IF((IC1D1+IC1D2+IC2D1+IC2D2+IC3D1+IC3D2),GT,0)GO TO 75
      WRITE(5,14)ITIME,IDATE
      GO TO 75
75      IC1D3=1
      IC2D1=1
76      WRITE(22,80)IDATE,ITIME,LINE,ITS,CT,ION,IOFF,
      2,IC1D1,IC1D2,IC1D3,IC2D1,IC2D2,IC2D3,IC3D1,IC3D2,IC3D3,ICOL
80      FORMAT(18,T4,A2,I1,A3,I3,I3,9(I1),2X,I1)
      GO TO 1
100     END

```

PROGRAM EDIT1

Program EDIT1 is similar to EDIT but is used for trains opening doors on both sides.

```

INTEGER LINE, CT, CAR1, CAR2, CAR3, D1, D2, D3, SIDE
CALL IFILE(21,'KEMOFE')
CALL OFILE(22,'SIKAI.')
10  IC1D1L=0
    IC1D2L=0
    IC1D3L=0
    IC2D1L=0
    IC2D2L=0
    IC2D3L=0
    IC3D1L=0
    IC3D2L=0
    IC3D3L=0
    IC1D1R=0
    IC1D2R=0
    IC1D3R=0
    IC2D1R=0
    IC2D2R=0
    IC2D3R=0
    IC3D1R=0
    IC3D2R=0
    IC3D3R=0
    READ(21,50,END=1000) IDATE, ITIME, LINE, ITS, CT, ION, IOFF, CAR1,
    2 CAR2, CAR3, D1, D2, D3, ICCL, SIDE
50  FORMAT(18,14,A2,I1,A3,2(I3),6(A1),2X,I1,A1)
    IF(CT.EQ.'PCC') GO TO 250
    IF(CAR1.EQ.'X'. AND. CAR2.EQ.'X'. AND. D1.EQ.'X'.
    2 AND .D3.EQ.'X') GO TO 700
    IF(CAR1.NE.'X') GO TO 70
    IF(SIDE.NE.'L') GO TO 61
    IF(D1.EQ.'X') IC1D1L=1
    IF(D2.EQ.'X') IC1D2L=1
    IF(D3.EQ.'X') IC1D3L=1
    GO TO 70
    IF(D1.NE.'X'. AND. D2.NE.'X'. AND. D3.NE.'X') GO TO 60
    GO TO 70
60  IC1D1L=1
    IC1D2L=1
    IC1D3L=1
    GO TO 70
61  IF(D1.EQ.'X') IC1D1R=1
    IF(D2.EQ.'X') IC1D2R=1
    IF(D3.EQ.'X') IC1D3R=1
    IF(D1.NE.'X'. AND. D2.NE.'X'. AND. D3.NE.'X') GO TO 62
    GO TO 70
62  IC1D1R=1
    IC1D2R=1
    IC1D3R=1
70  IF(CAR2.NE.'X') GO TO 90
    IF(SIDE.NE.'L') GO TO 81
    IF(D1.EQ.'X') IC2D1L=1
    IF(D2.EQ.'X') IC2D2L=1
    IF(D3.EQ.'X') IC2D3L=1
    IF(D1.NE.'X'. AND. D2.NE.'X'. AND. D3.NE.'X') GO TO 80
    GO TO 90
80  IC2D1L=1
    IC2D2L=1
    IC2D3L=1
    GO TO 90
81  IF(D1.EQ.'X') IC2D1R=1
    IF(D2.EQ.'X') IC2D2R=1
    IF(D3.EQ.'X') IC2D3R=1

```

PROGRAM EDIT1 (CONT.)

```

        IF (D1.NE.'X'.AND.D2.NE.'X'.AND.D3.NE.'X') GO TO 82
        GO TO 90
82      IC2D1R=1
        IC2D2R=1
        IC2D3R=1
90      IF (CAR1.NE.'X'.AND.CAR2.NE.'X'.AND.D1.NE.'X'.
2 AND.D2.NE.'X'.AND.D3.NE.'X') GO TO 100
        GO TO 120
100     IF (SIDE.NE.'L') GO TO 101
        IC1D1L=1
        IC1D2L=1
        IC1D3L=1
        IC2D1L=1
        IC2D2L=1
        IC2D3L=1
        GO TO 120
101     IC1D1R=1
        IC1D2R=1
        IC1D3R=1
        IC2D1R=1
        IC2D2R=1
        IC2D3R=1
120      IF ((IC1D1L+IC1D2L+IC1D3L+IC2D1L+IC2D2L+IC2D3L).GT.0.OR.
2 (IC1D1R+IC1D2R+IC1D3R+IC2D1R+IC2D2R+IC2D3R).GT.0)
2 GO TO 750
        WRITE(5,140) ITIME, IDATE
140      FORMAT('CANNOT ALLOCATE COUNT TO DOOR AT',1X,I4,
2 1X,'ON',1X,I8)
        GO TO 750
250     IF (CAR1.NE.'X') GO TO 270
        IF (SIDE.NE.'L') GO TO 265
        IF (D1.EQ.'X') IC1D1L=1
        IF (D2.EQ.'X') IC1D2L=1
        IF (D1.NE.'X'.AND.D2.NE.'X') GO TO 260
        GO TO 270
260     IC1D1L=1
        IC1D2L=1
        GO TO 270
265     IF (D1.EQ.'X') IC1D1R=1
        IF (D2.EQ.'X') IC1D2R=1
        IF (D1.NE.'X'.AND.D2.NE.'X') GO TO 266
        GO TO 270
266     IC1D1R=1
        IC1D2R=1
270      IF (CAR2.NE.'X') GO TO 290
        IF (SIDE.NE.'L') GO TO 281
        IF (D1.EQ.'X') IC2D1L=1
        IF (D2.EQ.'X') IC2D2L=1
        IF (D1.NE.'X'.AND.D2.NE.'X') GO TO 280
        GO TO 290
280     IC2D1L=1
        IC2D2L=1
        GO TO 290
281     IF (D1.EQ.'X') IC2D1R=1
        IF (D2.EQ.'X') IC2D2R=1
        IF (D1.NE.'X'.AND.D2.NE.'X') GO TO 282
        GO TO 290
282     IC2D1R=1
        IC2D2R=1
290      IF (CAR3.NE.'X') GO TO 310
        IF (SIDE.NE.'L') GO TO 305

```

PROGRAM EDIT1 (CONT.)

```

IF (D1.EQ.'X') IC3D1L=1
IF (D2.EQ.'X') IC3D2L=1
IF (D1.NE.'X'.AND.D2.NE.'X') GO TO 300
GO TO 310
300  IC3D1L=1
IC3D2L=1
GO TO 310
305  IF (D1.EQ.'X') IC3D1R=1
IF (D2.EQ.'X') IC3D2R=1
IF (D1.NE.'X'.AND.D2.NE.'X') GO TO 306
GO TO 310
306  IC3D1R=1
IC3D2R=1
IF (CAR1.NE.'X'.AND.CAR2.NE.'X'.AND.ITS.EQ.2.AND.D1.NE.'X'.
2 AND.D2.NE.'X') GO TO 330
GO TO 340
330  IF (SIDE.NE.'L') GO TO 335
IC1D1L=1
IC1D2L=1
IC2D1L=1
IC2D2L=1
GO TO 340
335  IC1D1R=1
IC1D2R=1
IC2D1R=1
IC2D2R=1
340  IF (CAR1.NE.'X'.AND.CAR2.NE.'X'.AND.CAR3.NE.'X'.AND.
2 ITS.EQ.3.AND.D1.NE.'X'.AND.D2.NE.'X') GO TO 370
GO TO 380
370  IF (SIDE.NE.'L') GO TO 375
IC1D1L=1
IC1D2L=1
IC2D1L=1
IC2D2L=1
IC3D1L=1
IC3D2L=1
GO TO 380
375  IC1D1R=1
IC1D2R=1
IC2D1R=1
IC2D2R=1
IC3D1R=1
IC3D2R=1
380  IF ((IC1D1L+IC1D2L+IC2D1L+IC2D2L+IC3D1L+IC3D2L).GT.0.
2 OR. (IC1D1R+IC1D2R+IC2D1R+IC2D2R+IC3D1R+IC3D2R).GT.0)
2 GO TO 750
WRITE(5,140) ITIME, IDATE
GO TO 750
700  IF (SIDE.NE.'L') GO TO 705
IC1D3L=1
IC2D1L=1
GO TO 750
705  IC1D3R=1
IC2D1R=1
750  WRITE(22,800) IDATE, ITIME, LINE, ITS, CT, ION, IOFF,
2 IC1D1L, IC1D2L, IC1D3L, IC2D1L, IC2D2L, IC2D3L,
2 IC3D1L, IC3D2L, IC3D3L, IC1D1R, IC1D2R, IC1D3R, IC2D1R, IC2D2R,
2 IC2D3R, IC3D1R, IC3D2R, IC3D3R, ICOL
800  FORMAT(I8,I4,A2,I1,A3,I3,I3,18(I1),2X,I1)
GO TO 10
1000 END

```


APPENDIX 5

PROGRAMS EDIT2 AND EDIT3

PROGRAM EDIT2

```

1      INTEGER LINE(0:4), ST(0:4)
2      DIMENSION ID1TB(0:4), IHP(0:4), IMIN(0:4), ITS(0:4),
2      ION(0:4), IDFF(0:4), IC1D1(0:4), IC1D2(0:4), IC1D3(0:4),
2      IC2D1(0:4), IC2D2(0:4), IC2D3(0:4), IC3D1(0:4), IC3D2(0:4),
2      IC3D3(0:4), TCOL(0:4), TCOUNT(0:4)
3      CALL IFILE(21,'STR11.')
4      CALL OFILF(22,'STR12.')
5      M=1
6      READ(21,5,END=500) ID1TB(M), IHP(M), IMIN(M), LINE(M), ITS(M),
7      ION(M), IDFF(M), IC1D1(M), IC1D2(M), IC1D3(M), IC2D1(M),
8      IC2D2(M), IC2D3(M), IC3D1(M), IC3D2(M), IC3D3(M), TCOL(M)
9      FORMAT(I8,2(I2),12,I1,A3,2(I3),9(I1),2X,I1)
10
11      DO 20 M=2,4
12      READ(21,5,END=23) IDATE(M), IHR(M), IMIN(M), LINE(M), ITS(M),
13      ST(M), ION(M), IDFF(M), IC1D1(M), IC1D2(M), IC1D3(M), IC2D1(M),
14      IC2D2(M), IC2D3(M), IC3D1(M), IC3D2(M), IC3D3(M), TCOL(M)
15      K=M
16
17      IF(((IHR(M)*60+IMIN(M))-(IHR(M-1)*60+IMIN(M-1))) .GT. 2)
18      GO TO 25
19      IF(IST(M).NE.IST(M-1)) GO TO 25
20      IF(ST(M).NE.ST(M-1)) GO TO 25
21      IF(ITS(M).NE.ITS(M-1)) GO TO 25
22      IF(TCOL(M).NE.TCOL(M-1)) GO TO 25
23      IF(M.LT.3) GO TO 20
24      IF(TCOL(M).EQ.TCOL(M-2).OR.TCOL(M).EQ.TCOL(M-3)) GO TO 25
25      CONTINUE
26
27      GO TO 24
28      IFT=1
29      IF(K.EQ.4) K=3
30      DO 30 M=1,K-1
31      ITCOUNT(M)=IC1D1(M)*100000000+IC1D2(M)*10000000+IC1D3(M)*1000000+
32      IC2D1(M)*100000+IC2D2(M)*10000+IC2D3(M)*1000+IC3D1(M)*100+
33      IC3D2(M)*10+IC3D3(M)
34      IF(ITCOUNT(M).EQ.0) ITCOUNT(M-1).AND.ION(M).EQ.ION(M-1)) 29,25
35      IF(M.LT.3) GO TO 28
36      IF(ITCOUNT(M).EQ.0) ITCOUNT(M-2).AND.ION(M).EQ.ION(M-2)) 29,27
37      IF(ITCOUNT(M).EQ.0) ITCOUNT(M-3).AND.ION(M).EQ.ION(M-3)) 29,28
38      ITCOUNT(M)=0
39      IC1D1(M)=0
40      IC1D2(M)=0
41      IC1D3(M)=0
42      IC2D1(M)=0
43      IC2D2(M)=0
44      IC2D3(M)=0
45      ION(M)=0
46      IDFF(M)=0
47      ITCOUNT=M=IDFF+IDFF(M)
48      DOOR=DOOR+IC1D1(M)+IC1D2(M)+IC1D3(M)+IC2D1(M)+IC2D2(M)+
49      IC2D3(M)+IC3D1(M)+IC3D2(M)+IC3D3(M)
50      ION=ION+ION(M)
51      IDFF=IDFF+IDFF(M)
52      CONTINUE
53
54      IF(MT(1).EQ.140.ITS(1).EQ.1) 40,50
55      IF(MT(1).EQ.110000000) 190,150

```

PROGRAM EDIT2 (CONT.)

```

50      IF(CT(1).EQ.'PCC').END.ITS(1).EQ.2) 60,70
60      IF(ITOTAL.EQ.1101110000) 190,160

70      IF(CT(1).EQ.'PCC').END.ITS(1).EQ.3) 80,90
80      IF(ITOTAL.EQ.1101110110) 190,170

90      IF(CT(1).EQ.'LRY').END.ITS(1).EQ.1) 100,110
100     IF(ITOTAL.EQ.1110000000) 190,180

110     IF(CT(1).EQ.'LRY').END.ITS(1).EQ.2) 120,500
120     IF(CT(1).EQ.'11110000) 190,170
130     LOFF=INT(TOFF/DOOF*2+.5)
140     LON=INT(TON/DOOF*2+.5)
150     GO TO 300
160     LOFF=INT(TOFF/DOOF*4+.5)
170     LON=INT(TON/DOOF*4+.5)
180     GO TO 300
190     LOFF=INT(TOFF/DOOF*6+.5)
200     LON=INT(TON/DOOF*6+.5)
210     GO TO 300
220     LOFF=INT(TOFF/DOOF*3+.5)
230     LON=INT(TON/DOOF*3+.5)
240     GO TO 300
250     LOFF=2000
260     LON=2000
270     TK=K-1
280     WPI'R(22,5) ED:TE(1),IAD(1),IMIN(1),LINE(1),ITS(1),CT(1),
290     ? LON,LOFF,IT
300     IF(IPI.EQ.1) GO TO 500
310     IT=0
320     K=0
330     NC=0
340     LOFF=0
350     IF(K.EQ.5) GO TO 1
360     ITF(1)=ITAD(1)
370     IAD(1)=ITF(K)
380     IMIN(1)=IMIN(K)
390     LINE(1)=LINE(K)
400     ITS(1)=ITS(K)
410     CT(1)=CT(K)
420     LON(1)=LON(K)
430     LOFF(1)=TOFF(K)
440     IT1D1(1)=IT1D1(K)
450     IT1D2(1)=IT1D2(K)
460     IT1D3(1)=IT1D3(K)
470     IT2D1(1)=IT2D1(K)
480     IT2D2(1)=IT2D2(K)
490     IT2D3(1)=IT2D3(K)
500     IT3D1(1)=IT3D1(K)
510     IT3D2(1)=IT3D2(K)
520     IT3D3(1)=IT3D3(K)
530     ITOL(1)=ITOL(K)
540     GO TO 2
550     END

```

PROGRAM EDIT3

Program EDIT3 is similar to EDIT2 but is used for trains opening doors on both sides.

```

1      IF(EGFS LINE(0:4),CT(0:4))
2      DIMENSION IDATE(0:4),IHR(0:4),IMIN(0:4),ITS(0:4),
2      IDN(0:4),IOFF(0:4),IC1D1L(0:4),IC1D2L(0:4),IC1D3L(0:4),
2      IC2D1L(0:4),IC2D2L(0:4),IC2D3L(0:4),IC3D1L(0:4),IC3D2L(0:4),
2      IC3D3L(0:4),IC1D1R(0:4),IC1D2R(0:4),IC1D3R(0:4),IC2D1R(0:4),
2      IC2D2R(0:4),IC2D3R(0:4),IC3D1R(0:4),IC3D2R(0:4),IC3D3R(0:4),
2      ICOL(0:4),ICOUNT(0:4)
3      CALL IFILE(21,'STRA1.')
4      CALL OFILE(22,'STRA2.')
1      M=1
5      READ(21,5,END=500)IDATE("),IHR(M),IMIN(M),LINE(M),ITS(M),
2      CT(M),IDN(M),IOFF(M),IC1D1L(M),IC1D2L(M),IC1D3L(M),IC2D1L(M),
2      IC2D2L(M),IC2D3L(M),IC3D1L(M),IC3D2L(M),IC3D3L(M),IC1D1R(M),
2      IC1D2R(M),IC1D3R(M),IC2D1R(M),IC2D2R(M),IC2D3R(M),IC3D1R(M),
2      IC3D2R(M),IC3D3R(M),ICOL(M)
5      FORMAT(18,2(I2),A2,II,A3,2(I3),9(I1),9(I1),2X,I1)

2      DO 20 M=2,4
3      READ(21,5,END=23)IDATE("),IHR(M),IMIN(M),LINE(M),ITS(M),
2      CT(M),IDN(M),IOFF(M),IC1D1L(M),IC1D2L(M),IC1D3L(M),IC2D1L(M),
2      IC2D2L(M),IC2D3L(M),IC3D1L(M),IC3D2L(M),IC3D3L(M),
2      IC1D1R(M),IC1D2R(M),IC1D3R(M),IC2D1R(M),IC2D2R(M),IC2D3R(M),
2      IC3D1R(M),IC3D2R(M),IC3D3R(M),ICOL(M)
K=M

15     IF(((IHR(M)*60+IMIN(M))-(IHR(M-1)*60+IMIN(M-1))).GT.2)
2      GO TO 25
16     IF(LINE(M).NE.LINE(M-1))GO TO 25
17     IF(CT(M).NE.CT(M-1))GO TO 25
18     IF(ITS(M).NE.ITS(M-1))GO TO 25
19     IF(ICOL(M).EQ.ICOL(M-1))GO TO 25
20     IF(M.LT.3)GO TO 20
21     IF(ICOL(M).EQ.ICOL(M-2).OR.ICOL(M).EQ.ICOL(M-3))GO TO 25
22     CONTINUE

23     GO TO 24
23     IF I=1
24     IF(K.FQ.4)K=5
25     DO 30 M=1,K-1
30     ICOUNT(M)=IC1D1L(M)*10**17+IC1D2L(M)*10**16+IC1D3L(M)*10**15+
2      IC2D1L(M)*10**14+IC2D2L(M)*10**13+IC2D3L(M)*10**12+
2      IC3D1L(M)*10**11+IC3D2L(M)*10**10+IC3D3L(M)*10**9+IC1D1R(M)*
2      10**8+IC1D2R(M)*10**7+IC1D3R(M)*10**6+IC2D1R(M)*10**5+
2      IC2D2R(M)*10**4+IC2D3R(M)*10**3+IC3D1R(M)*10**2+
2      IC3D2R(M)*10+IC3D3R(M)
31     IF(ICOUNT(M).EQ.ICOUNT(M-1).AND.ION(M).EQ.ION(M-1))29,26
26     IF(M.LT.3)GO TO 28
27     IF(ICOUNT(M).EQ.ICOUNT(M-2).AND.ION(M).EQ.ION(M-2))29,27
28     IF(ICOUNT(M).EQ.ICOUNT(M-3).AND.ION(M).EQ.ION(M-3))29,28
29     ICOUNT(M)=0
30     IC1D1L(M)=0
31     IC1D2L(M)=0
32     IC1D3L(M)=0
33     IC2D1L(M)=0
34     IC2D2L(M)=0
35     IC2D3L(M)=0
36     IC3D1L(M)=0
37     IC3D2L(M)=0
38     IC3D3L(M)=0
39     IC1D1R(M)=0
40     IC1D2R(M)=0

```

PROGRAM EDIT3 (CONT.)

```

----- IC1D3R(M)=0 -----
----- IC2D1P(M)=0 -----
----- IC2D2E(M)=0 -----
----- IC2D3R(M)=0 -----
----- IC3D1P(M)=0 -----
----- IC3D2R(M)=0 -----
----- IC3D3P(M)=0 -----
----- ION(M)=0 -----
----- TOFF1M=0
28   ITOTAL=ITOTAL+ICCOUNT(M)
      DOOR=DOOR+IC1D1L(M)+IC1D2L(M)+IC2D1L(M)+IC2D2L(M)+_
      ? IC2D3L(M)+IC3D1L(M)+IC3D2L(M)+IC3D3L(M)+IC1D1P(M)+_
      ? IC1D2R(M)+IC1D3R(M)+IC2D1R(M)+IC2D2R(M)+IC2D3R(M)+_
      ? IC3D1F(M)+IC3D2P(M)+IC3D3R(M)
      TON=TON+ION(M)
      TOFF=TOFF+TOFF1M
30   CONTINUE
      IF(CT(1).EQ.'PCC'.AND.ITS(1).EQ.1)40,50
40   IF(ITOTAL.EQ.111*10**16+11*10**7)111190,150
      IF(CT(1).EQ.'PCC'.AND.ITS(1).EQ.2)160,70
      IF(ITOTAL.EQ.(111*10**16+11*10**13+11*10**7+11*10**4))190,150
      IF(CT(1).EQ.'PCC'.AND.ITS(1).EQ.3)80,90
50   IF(ITOTAL.EQ.(111*10**16+11*10**13+_
      ? 11*10**10+11*10**7+11*10**4+110))190,170
      IF(CT(1).EQ.'LRV'.AND.ITS(1).EQ.1)100,110
100  IF(ITOTAL.EQ.111000000)190,180
      ? 111*10**15+111*10**6
110  IF(CT(1).EQ.'LRV'.AND.ITS(1).EQ.2)120,500
120  IF(ITOTAL.EQ.(111111*10**11+111111*10**3))190,170
130  LOFF=INT(TOFF/DOOR*4+.5)
      LON=INT(TON/DOOR*4+.5)
      GO TO 300
140  LOFF=INT(TOFF/DOOR*8+.5)
      LON=INT(TON/DOOR*8+.5)
      GO TO 300
150  LOFF=INT(TOFF/DOOR*12+.5)
      LON=INT(TON/DOOR*12+.5)
      GO TO 300
160  LOFF=INT(TOFF/DOOR*6+.5)
      LON=INT(TON/DOOR*6+.5)
      GO TO 300
170  LOFF=TCFF
      LON=TON
180  IK=K-1
      WRITE(22,5)IDATE(1),IHR(1),IMIN(1),LINE(1),ITS(1),CT(1),
      ? LCN,LOFF,IK
      IF(IF1.EQ.1)GO TO 500
      ITOTAL=0
      DOOR=0
      TON=0
      TOFF=0
      IF(K.EQ.5)GO TO 1
      IDATE(1)=IDATE(K)
      IHR(1)=IHR(K)
      IMIN(1)=IMIN(K)
      LINE(1)=LINE(K)

```

PROGRAM EDIT3 (CONT.)

```
ITS(1)=ITS(K)
CT(1)=CT(K)
ITN(1)=ITN(K)
ITFF(1)=ITFF(K)
IC1D1L(1)=IC1D1L(K)
IC1D2L(1)=IC1D2L(K)
IC1D3L(1)=IC1D3L(K)
IC2D1L(1)=IC2D1L(K)
IC2D2L(1)=IC2D2L(K)
IC2D3L(1)=IC2D3L(K)
IC2D1L(1)=IC2D1L(K)
IC3D2L(1)=IC3D2L(K)
IC3D3L(1)=IC3D3L(K)
IC1D1R(1)=IC1D1R(K)
IC1D2R(1)=IC1D2R(K)
IC1D3R(1)=IC1D3R(K)
IC2D1R(1)=IC2D1R(K)
IC2D2R(1)=IC2D2R(K)
IC2D3R(1)=IC2D3R(K)
IC3D1R(1)=IC3D1R(K)
IC3D2R(1)=IC3D2R(K)
IC3D3R(1)=IC3D3R(K)
ICOL(1)=ICOL(K)
END
```

500

END

APPENDIX 6 PROGRAM SEPAR

Program SEPAR sorts the data into two inbound and outbound files.

```
OPEN F1.FIL.  
F1.I1.  
INI 1 PAKLEC.  
DPI START.  
L1: GETREC LB.  
IF DONE LT 7 THEN L2.  
GOTO L1.  
L2: CHANGE HOUR HOUR+12.  
GO TO L1.  
L3: DPI END.  
FIND LINE EQ "L" OR "G0" OR "N" OR "P".  
SOFT BY NOTE MIN.  
PRINT ON 1 MYDAY HOUR MIN LINE TPA*INSIZE TYPEOPTAR 6  
$ASSON $ASSON COLLECT FMT D4 I2 I2 A2 I1 A3 I3 I3 1X I1 END.  
FIND NOT I'ST.  
SOFT BY NOTE MIN.  
INTE 2 PAKRIV.  
PRINT 0" 2 MYDAY HOUR MIN LINE TPA*INSIZE TYPEOPTAR 6  
$ASSON $ASSON COLLECT FFORMAT D4 I2 I2 A2 6  
I1 A2 I3 I3 1X I1 END.  
DPIE.
```


APPENDIX 7
FINAL OUTPUTS: PAKRIV AND PAKLEC
PAKRIV

| Date | Time | Line | Train size | On | Off | # of Surveyor |
|----------|------------|----------|------------|----|-----|---------------|
| 19780522 | 7 08 | 2LPAV | 3 | 0 | 2 | 2 |
| 19780522 | 710P | 21RV | 14 | 0 | 2 | 2 |
| 19780522 | 715P | 2LPAV | 0 | 0 | 2 | 2 |
| 19780522 | 7178C2PCC | 0 | 0 | 2 | 2 | 2 |
| 19780522 | 7180C2PCC | 0 | 0 | 2 | 2 | 2 |
| 19780522 | 720P | 21RV | 5P | 11 | 2 | 2 |
| 19780522 | 722P | 1PCC | 0 | 0 | 2 | 2 |
| 19780522 | 723P | 1PCC | 0 | 0 | 2 | 2 |
| 19780522 | 7258C2PCC | 0 | 0 | 2 | 2 | 2 |
| 19780522 | 725P | 21EV | 9 | 7 | 2 | 2 |
| 19780522 | 725P | 1PCC | 0 | 0 | 2 | 2 |
| 19780522 | 7261 | 11PAV | 0 | 0 | 1 | 1 |
| 19780522 | 726P | 12PCC | 0 | 0 | 1 | 1 |
| 19780522 | 726P | 11PAV | 0 | 0 | 1 | 1 |
| 19780522 | 727P | 2LPAV | 5 | 7 | 2 | 2 |
| 19780522 | 7287C2PCC | 0 | 0 | 2 | 2 | 2 |
| 19780522 | 733P | 1PCC | 0 | 0 | 2 | 2 |
| 19780522 | 7348C2PCC | 0 | 0 | 2 | 2 | 2 |
| 19780522 | 7350C2PCC | 0 | 0 | 2 | 2 | 2 |
| 19780522 | 740P | 21RV142 | 34 | 4 | 4 | 4 |
| 19780522 | 7417C2LPAV | 0 | 0 | 4 | 4 | 4 |
| 19780522 | 748P | 1PCC | 0 | 0 | 4 | 4 |
| 19780522 | 749772PCC | 0 | 0 | 4 | 4 | 4 |
| 19780522 | 750P | 1PCC | 0 | 0 | 4 | 4 |
| 19780522 | 7518C1LPAV | 0 | 0 | 3 | 3 | 3 |
| 19780522 | 751P | 11PAV | 0 | 0 | 3 | 3 |
| 19780522 | 752P | 1PCC | 0 | 0 | 1 | 1 |
| 19780522 | 752P | 11RV | 0 | 0 | 2 | 2 |
| 19780522 | 753P | 2LPAV110 | 24 | 4 | 4 | 4 |
| 19780522 | 753P | 11PAV | 0 | 0 | 1 | 1 |
| 19780522 | 755P | 1PCC | 0 | 0 | 3 | 3 |
| 19780522 | 7558C21PAV | 0 | 0 | 3 | 3 | 3 |
| 19780522 | 7560C1LPAV | 0 | 0 | 1 | 1 | 1 |
| 19780522 | 7567721PAV | 0 | 0 | 1 | 1 | 1 |
| 19780522 | 756P | 1PCC | 0 | 0 | 4 | 4 |
| 19780522 | 756P | 21PAV | 2 | 1 | 3 | 3 |
| 19780522 | 757P | 2LPAV | 0 | 0 | 2 | 2 |
| 19780522 | 758P | 1PCC | 0 | 0 | 2 | 2 |
| 19780522 | 8 00C2PCC | 0 | 0 | 4 | 4 | 4 |
| 19780522 | 8 18 | 21PAV | 23 | 31 | 4 | 4 |
| 19780522 | 8 49 | 1PCC | 0 | 0 | 4 | 4 |
| 19780522 | 8 57C2PCC | 0 | 0 | 4 | 4 | 4 |
| 19780522 | 8 58C3PCC | 0 | 0 | 4 | 4 | 4 |
| 19780522 | 8 69 | 21PAV | 0 | 0 | 1 | 1 |
| 19780522 | 8 69 | 11PAV | 0 | 0 | 2 | 2 |
| 19780522 | 8 79 | 11PAV | 0 | 0 | 1 | 1 |
| 19780522 | 8 88 | 1LPAV | 0 | 0 | 4 | 4 |
| 19780522 | 810P | 1PCC | 0 | 0 | 2 | 2 |
| 19780522 | 8108C2PCC | 0 | 0 | 4 | 4 | 4 |
| 19780522 | 812P | 21PAV121 | 21 | 4 | 4 | 4 |
| 19780522 | 8128C2PCC | 0 | 0 | 4 | 4 | 4 |
| 19780522 | 814P | 11PAV | 0 | 0 | 1 | 1 |
| 19780522 | 815P | 1PCC | 0 | 0 | 2 | 2 |
| 19780522 | 8157C2PCC | 0 | 0 | 1 | 1 | 1 |
| 19780522 | 815P | 1PCC | 0 | 0 | 2 | 2 |
| 19780522 | 816P | 1PCC | 0 | 0 | 1 | 1 |
| 19780522 | 816P | 1PCC | 0 | 0 | 3 | 3 |
| 19780522 | 817P | 21PAV | 21 | 41 | 4 | 4 |
| 19780522 | 822P | 1PCC | 0 | 0 | 4 | 4 |
| 19780522 | 824P | 21PAV118 | 35 | 4 | 4 | 4 |
| 19780522 | 826P | 1PCC | 0 | 0 | 4 | 4 |

PAKLEC

| Date | Time | Line | Train-size | On | Off | # of Surveyors |
|----------|-------|-------------|------------|-----|-----|----------------|
| 19780524 | 7303 | 71PVA | 2 | 2 | 2 | 2 |
| 19780524 | 721N | 2LPA | 75 | 36 | 2 | |
| 19780524 | 735G | 1PVA | 2 | 2 | 2 | |
| 19780524 | 738P | 1LPA | 2 | 2 | 1 | |
| 19780524 | 739L | 3PVA130162 | 2 | | | |
| 19780524 | 7403 | 3PVA | 3 | 0 | 1 | |
| 19780524 | 7413 | 11PVA | 2 | 2 | 2 | |
| 19780524 | 742N | 2LPA | 35 | 73 | 2 | |
| 19780524 | 743L | 3PVA | 22 | 49 | 2 | |
| 19780524 | 7443 | 3PVA | 2 | 2 | 2 | |
| 19780524 | 748P | 21PVA | 24138 | 1 | | |
| 19780524 | 748L | 2LPA | 80168 | 2 | | |
| 19780524 | 7483 | 1PVA | 2 | 2 | 2 | |
| 19780524 | 7493 | 3PVA | 2 | 2 | 1 | |
| 19780524 | 750L | 2LPA | 66 | 54 | 1 | |
| 19780524 | 753N | 21PVA105213 | 2 | | | |
| 19780524 | 755L | 3PVA | 15 | 67 | 2 | |
| 19780524 | 757N | 2LPA | 15101 | 2 | | |
| 19780524 | 758G | 1PVA | 2 | 2 | 2 | |
| 19780524 | 758N | 21PVA | 1 | 26 | 2 | |
| 19780524 | 8 0N | 2LPA | 57 | 79 | 3 | |
| 19780524 | 8 4N | 3PVA | 2 | 2 | 4 | |
| 19780524 | 8 4L | 2PVA | 43100 | 3 | | |
| 19780524 | 8 5L | 3PVA | 15 | 65 | 4 | |
| 19780524 | 8 53 | 1PVA | 2 | 2 | 4 | |
| 19780524 | 8 6P | 2PVA | 3 | 54 | 4 | |
| 19780524 | 8 73 | 1PVA | 2 | 2 | 4 | |
| 19780524 | 8 86 | 3PVA | 2 | 2 | 4 | |
| 19780524 | 8 14P | 21PVA | 62100 | 4 | | |
| 19780524 | 815L | 3PVA | 3 | 99 | 4 | |
| 19780524 | 816L | 2PVA | 45 | 73 | 4 | |
| 19780524 | 8173 | 1PVA | 2 | 2 | 3 | |
| 19780524 | 818L | 2PVA | 2110 | 4 | | |
| 19780524 | 819N | 11PVA | 2 | 92 | 4 | |
| 19780524 | 8203 | 1PVA | 2 | 2 | 4 | |
| 19780524 | 8243 | 3PVA | 2 | 2 | 4 | |
| 19780524 | 826L | 2PVA | 52 | 27 | 4 | |
| 19780524 | 827L | 2PVA | 1 | 62 | 4 | |
| 19780524 | 8293 | 1PVA | 2 | 2 | 4 | |
| 19780524 | 829N | 11PVA | 11 | 11 | 4 | |
| 19780524 | 8303 | 1PVA | 2 | 2 | 4 | |
| 19780524 | 830P | 11PVA | 2 | 2 | 1 | |
| 19780524 | 8303 | 1PVA | 2 | 2 | 4 | |
| 19780524 | 8323 | 3PVA | 2 | 2 | 4 | |
| 19780524 | 835L | 2PVA | 65 | 101 | 4 | |
| 19780524 | 836N | 21PVA | 2120 | 4 | | |
| 19780524 | 8263 | 2PVA | 2 | 2 | 4 | |
| 19780524 | 828L | 2PVA | 34 | 112 | 4 | |
| 19780524 | 8403 | 1PVA | 2 | 2 | 4 | |
| 19780524 | 8411 | 3PVA | 4 | 95 | 4 | |
| 19780524 | 842P | 11PVA | 2 | 88 | 4 | |
| 19780524 | 8433 | 1PVA | 2 | 2 | 3 | |
| 19780524 | 846L | 2PVA | 24 | 110 | 4 | |
| 19780524 | 847P | 11PVA | 2 | 2 | 1 | |
| 19780524 | 8473 | 1PVA | 2 | 2 | 3 | |
| 19780524 | 848N | 11PVA | 2 | 46 | 4 | |
| 19780524 | 850L | 2PVA | 2 | 51 | 4 | |
| 19780524 | 8523 | 1PVA | 2 | 2 | 4 | |
| 19780524 | 852L | 2PVA | 121 | 04 | 4 | |
| 19780524 | 8523 | 3PVA | 2 | 2 | 3 | |

APPENDIX 8 PROGRAM PROPFL

Program PROPFL generates the actual time series of the observed data for individual stations.

```

1.      INTEGER ITRAIN(500)
2.      DIMENSION IHR(500),IMIN(500),ION(500),IOFF(500)
3.      DOUBLE PRECISION FILEIN, FILEOUT, DIR, STAT
4.      TYPE 5
5.      FORMAT('INPUT FILE NAME =',S)
6.      ACCEPT 6, FILEIN
7.      TYPE 4
8.      FORMAT('OUTPUT FILE NAME = ',S)
9.      ACCEPT 6, FILEOUT
10.     FORMAT(A10)
11.     OPTN(UNIT=21,DEVICE='DSK',ACCESS='SEQIN',FILE=FILEIN)
12.     OPEN(UNIT=22,DEVICE='DSK',ACCESS='SEQOUT',FILE=FILEOUT)
13.     TYPE 7
14.     FORMAT('TO WHAT DIRECTION?',1X,S)
15.     ACCEPT 8,DIR
16.     FORMAT(A10)
17.     TYPE 8
18.     FORMAT ('AT WHAT STATION?',1X,S)
19.     ACCEPT 10,STAT
20.     FORMAT(A10)
21.     WRITE(22,11) STAT,DIR
22.     WRITE (22,12)
23.     FORMAT(//2X,'TIME',2X,'HEADWAY',2X,'PASS ON',1X,'ON RATE',
24.           2 1X,'PASS OFF',1X,'OFF RATE',2X,'TRAIN IN BKT')
25.     N=0
26.     ITIME=0
27.     DO 100 I=1,500
28.     READ(21,20,END=500) IHR(I),IMIN(I),ITRAIN(I),ION(I),
29.           2 IOFF(I)
30.     FORMAT(8X,I2,I2,'2',4X,I3,I3,2X)
31.     PASON=ION(I)
32.     PASOFF=IOFF(I)
33.     NUM=I-N-1
34.     IF(DIR.EQ.'LECHKEPE') GO TO 23
35.     IF(ITRAIN(I).EQ.'E') 23,100
36.     HEDWAY=(IHR(I)*60+IMIN(I))-ITIME
37.     PEDWAY=HEDWAY
38.     IF(HEDWAY.EQ.0) PEDWAY=1
39.     FACTION=PASON/PEDWAY
40.     RATEOF=PASOFF/PEDWAY
41.     WRITE(22,50) IHR(I),IMIN(I),HEDWAY,ION(I),FACTION,IOFF(I),
42.           2 FACTION,NUM
43.     FORMAT(1X,'AT STATION=',1X,A10,'GOING TO',1X,A10)
44.     FORMAT(2X,I2,I2,4X,F5.1,5X,I3,5X,F4.1,
45.           25X,I3,5X,F4.1,8X,I2)
46.     ITIME=IHR(I)*60+IMIN(I)
47.     N=I
48.     CONTINUE
49. 100
50. 500
500      END

```


APPENDIX 9
STATION PROFILE: PAKPFL

AT STATION = PARK ST. GOING TO RIVERSIDE

| TIME | HEADWAY | PASS | ON | OFF | PASS | OFF | OFF | RATE | TRAIN IN | BET |
|------|---------|------|------|-----|------|------|-----|------|----------|-----|
| 7:0 | 420.0* | 3 | 7.0 | | 2 | 0.0 | | 0.0 | 0 | |
| 710 | 10.0 | 4 | 1.4 | | 8 | 0.8 | | 0.8 | 0 | |
| 720 | 10.0 | 53 | 5.8 | | 11 | 1.1 | | 1.1 | 3 | |
| 725 | 5.0 | 9 | 1.8 | | 7 | 1.4 | | 1.4 | 3 | |
| 727 | 2.0 | 5 | 3.0 | | 7 | 3.5 | | 3.5 | 4 | |
| 740 | 12.0 | 142 | 10.9 | | 34 | 2.6 | | 2.6 | 4 | |
| 753 | 13.0 | 112 | 3.5 | | 24 | 1.3 | | 1.3 | 3 | |
| 756 | 3.0 | 2 | 0.7 | | 1 | 0.3 | | 0.3 | 5 | |
| 757 | 1.0 | 2 | 2.0 | | 0 | 0.0 | | 0.0 | 3 | |
| 8:1 | 4.0 | 22 | 3.3 | | 31 | 7.3 | | 7.3 | 2 | |
| 812 | 11.0 | 120 | 10.9 | | 21 | 1.9 | | 1.9 | 9 | |
| 817 | 5.0 | 21 | 18.2 | | 41 | 8.2 | | 8.2 | 7 | |
| 824 | 7.0 | 118 | 15.9 | | 35 | 5.0 | | 5.0 | 1 | |
| 840 | 15.0 | 34 | 5.9 | | 30 | 1.3 | | 1.3 | 7 | |
| 847 | 7.0 | 47 | 5.7 | | 42 | 6.0 | | 6.0 | 9 | |
| 848 | 1.0 | 32 | 23.0 | | 21 | 21.0 | | 21.0 | 0 | |
| 854 | 5.0 | 15 | 2.7 | | 3 | 0.5 | | 0.5 | 4 | |
| 860 | 15.0 | 54 | 3.6 | | 11 | 0.7 | | 0.7 | 20 | |
| 911 | 2.0 | 25 | 12.5 | | 2 | 1.0 | | 1.0 | 3 | |
| 915 | 4.0 | 29 | 9.8 | | 8 | 2.0 | | 2.0 | 1 | |
| 928 | 13.0 | 24 | 1.8 | | 39 | 3.0 | | 3.0 | 9 | |
| 934 | 5.0 | 28 | 5.3 | | 23 | 3.3 | | 3.3 | 5 | |
| 940 | 5.0 | 21 | 3.5 | | 5 | 1.0 | | 1.0 | 5 | |
| 950 | 10.0 | 22 | 2.2 | | 57 | 5.7 | | 5.7 | 7 | |
| 956 | 5.0 | 17 | 2.8 | | 5 | 0.8 | | 0.8 | 7 | |
| 1012 | 15.0 | 70 | 2.4 | | 10 | 0.6 | | 0.6 | 7 | |
| 1024 | 12.0 | 74 | 5.2 | | 0 | 0.0 | | 0.0 | 3 | |
| 1025 | 1.0 | 12 | 12.0 | | 6 | 9.0 | | 9.0 | 2 | |
| 1026 | 1.0 | 12 | 12.0 | | 14 | 14.0 | | 14.0 | 9 | |
| 1224 | 183.0* | 72 | 0.4 | | 12 | 0.1 | | 0.1 | 5 | |
| 1242 | 3.0 | 22 | 2.5 | | 15 | 1.9 | | 1.9 | 4 | |
| 1255 | 12.0 | 20 | 5.9 | | 39 | 3.0 | | 3.0 | 2 | |
| 1259 | 4.0 | 21 | 5.3 | | 33 | 8.3 | | 8.3 | 2 | |
| 1415 | 5.0 | 15 | 2.5 | | 18 | 3.0 | | 3.0 | 4 | |
| 1412 | 7.0 | 72 | 10.3 | | 24 | 3.4 | | 3.4 | 1 | |
| 1423 | 11.0 | 24 | 2.2 | | 6 | 0.5 | | 0.5 | 3 | |
| 1428 | 5.0 | 21 | 4.2 | | 18 | 3.5 | | 3.5 | 5 | |
| 1441 | 12.0 | 102 | 7.8 | | 21 | 1.5 | | 1.5 | 7 | |
| 1448 | 7.0 | 25 | 2.6 | | 4 | 0.6 | | 0.6 | 4 | |
| 1459 | 11.0 | 21 | 5.9 | | 33 | 3.0 | | 3.0 | 6 | |
| 1513 | 4.0 | 29 | 7.3 | | 7 | 1.3 | | 1.3 | 3 | |
| 1512 | 9.0 | 147 | 13.0 | | 78 | 8.7 | | 8.7 | 12 | |
| 1523 | 11.0 | 82 | 3.4 | | 58 | 6.2 | | 6.2 | 11 | |
| 1526 | 2.0 | 25 | 31.7 | | 36 | 12.0 | | 12.0 | 2 | |
| 1532 | 5.0 | 11 | 1.8 | | 30 | 5.0 | | 5.0 | 4 | |
| 1534 | 2.0 | 14 | 7.0 | | 4 | 2.0 | | 2.0 | 3 | |
| 1537 | 2.0 | 16 | 5.3 | | 14 | 4.7 | | 4.7 | 2 | |
| 1540 | 12.0 | 62 | 5.3 | | 17 | 1.4 | | 1.4 | 5 | |
| 1555 | 5.0 | 45 | 7.5 | | 33 | 5.5 | | 5.5 | 5 | |
| 1555 | 10.0 | 50 | 5.0 | | 15 | 1.5 | | 1.5 | 5 | |
| 1615 | 12.0 | 50 | 5.9 | | 29 | 2.9 | | 2.9 | 8 | |
| 1618 | 2.0 | 49 | 15.0 | | 57 | 19.0 | | 19.0 | 0 | |
| 1627 | 2.0 | 52 | 6.7 | | 29 | 3.2 | | 3.2 | 8 | |
| 1630 | 2.0 | 52 | 10.7 | | 21 | 7.0 | | 7.0 | 2 | |
| 1641 | 11.0 | 221 | 20.1 | | 186 | 16.9 | | 16.9 | 3 | |
| 1652 | 11.0 | 122 | 2.3 | | 10 | 1.7 | | 1.7 | 10 | |
| 1655 | 2.0 | 55 | 22.0 | | 14 | 4.7 | | 4.7 | 3 | |

* large headways indicate break in data

STATION PROFILE: PAKPFL (CONT.)

| | | | | | | |
|------|------|-----|------|----|------|----|
| 1711 | 15.0 | 111 | 5.9 | 0 | 5.0 | 5 |
| 1718 | 7.0 | 112 | 15.1 | 51 | 7.3 | 4 |
| 1721 | 3.0 | 133 | 52.7 | 92 | 30.7 | 2 |
| 1726 | 5.0 | 56 | 13.2 | 17 | 3.4 | 5 |
| 1730 | 4.0 | 25 | 5.5 | 16 | 4.0 | 3 |
| 1730 | 0.0 | 29 | 22.0 | 12 | 12.0 | 0 |
| 1731 | 1.0 | 41 | 41.0 | 29 | 29.0 | 0 |
| 1733 | 2.0 | 22 | 11.0 | 40 | 20.0 | 3 |
| 1742 | 3.0 | 37 | 3.7 | 9 | 1.0 | 6 |
| 1744 | 2.0 | 0 | 4.5 | 4 | 2.0 | 2 |
| 18 0 | 15.0 | 113 | 7.4 | 38 | 2.4 | 12 |
| 18 6 | 5.0 | 32 | 5.2 | 48 | 8.0 | 2 |
| 18 8 | 2.0 | 33 | 15.0 | 2 | 1.0 | 3 |
| 19 0 | 2.0 | 46 | 23.0 | 7 | 3.5 | 0 |

STATION PROFILE: PAKPFL (CONT.)

AT STATION = PK ST. GOING TO NORTH STATION

| LINE | HEADWAY | PASS ON | ON TIME | PASS | OFF | OFF TIME | I | IN | IN | BET |
|------|---------|---------|---------|------|------|----------|---|----|----|-----|
| 731 | 451.0 | 75 | 0.2 | 36 | 0.1 | | | 1 | | |
| 742 | 11.0 | 25 | 2.3 | 78 | 7.1 | | | 5 | | |
| 748 | 6.0 | 24 | 4.0 | 138 | 23.0 | | | 2 | | |
| 753 | 5.0 | 106 | 21.2 | 215 | 43.0 | | | 5 | | |
| 757 | 4.0 | 15 | 3.8 | 101 | 25.3 | | | 1 | | |
| 758 | 1.0 | 1 | 1.0 | 26 | 26.0 | | | 1 | | |
| 8 0 | 2.0 | 52 | 26.5 | 79 | 39.5 | | | 0 | | |
| 814 | 14.0 | 62 | 4.5 | 109 | 7.8 | | | 7 | | |
| 815 | 5.0 | 1 | 0.4 | 90 | 18.0 | | | 4 | | |
| 829 | 10.0 | 1 | 0.1 | 111 | 11.1 | | | 5 | | |
| 836 | 7.0 | 2 | 0.3 | 130 | 18.6 | | | 5 | | |
| 842 | 5.0 | 5 | 0.0 | 68 | 14.7 | | | 4 | | |
| 848 | 6.0 | 3 | 0.5 | 46 | 7.7 | | | 4 | | |
| 850 | 6.0 | 12 | 1.5 | 89 | 11.1 | | | 7 | | |
| 919 | 23.0 | 1 | 0.0 | 26 | 1.1 | | | 14 | | |
| 922 | 7.0 | 7 | 2.3 | 46 | 15.3 | | | 5 | | |
| 928 | 6.0 | 13 | 2.2 | 75 | 12.5 | | | 6 | | |
| 930 | 2.0 | 6 | 2.0 | 42 | 21.0 | | | 2 | | |
| 940 | 10.0 | 0 | 0.0 | 59 | 5.9 | | | 8 | | |
| 949 | 9.0 | 6 | 0.7 | 42 | 4.7 | | | 7 | | |
| 954 | 5.0 | 10 | 2.2 | 70 | 14.0 | | | 2 | | |
| 959 | 9.0 | 13 | 2.6 | 60 | 16.0 | | | 2 | | |
| 10 9 | 10.0 | 0 | 0.0 | 38 | 3.8 | | | 5 | | |
| 1014 | 5.0 | 11 | 2.2 | 46 | 9.2 | | | 3 | | |
| 1027 | 13.0 | 17 | 1.3 | 59 | 4.5 | | | 6 | | |
| 1039 | 12.0 | 8 | 2.7 | 59 | 4.0 | | | 5 | | |
| 1051 | 12.0 | 9 | 0.8 | 115 | 9.6 | | | 3 | | |
| 1058 | 7.0 | 6 | 1.1 | 49 | 7.0 | | | 3 | | |
| 1524 | 260.0 | 324 | 1.2 | 312 | 1.2 | | | 4 | | |
| 1530 | 6.0 | 30 | 5.0 | 62 | 10.0 | | | 2 | | |
| 1543 | 10.0 | 34 | 2.6 | 46 | 3.5 | | | 11 | | |
| 1544 | 1.0 | 0 | 6.0 | 79 | 79.0 | | | 0 | | |
| 1550 | 6.0 | 14 | 2.0 | 93 | 15.5 | | | 4 | | |
| 16 0 | 10.0 | 0 | 0.0 | 27 | 2.7 | | | 10 | | |
| 1610 | 10.0 | 92 | 5.2 | 206 | 20.6 | | | 1 | | |
| 1618 | 6.0 | 32 | 4.9 | 39 | 4.9 | | | 4 | | |
| 1621 | 3.0 | 22 | 7.3 | 74 | 24.7 | | | 3 | | |
| 1627 | 5.0 | 14 | 2.3 | 114 | 19.3 | | | 7 | | |
| 1634 | 7.0 | 19 | 2.7 | 132 | 18.9 | | | 6 | | |
| 1637 | 3.0 | 11 | 3.7 | 53 | 17.7 | | | 2 | | |
| 1648 | 11.0 | 8 | 0.7 | 52 | 4.7 | | | 4 | | |
| 17 0 | 12.0 | 34 | 2.8 | 103 | 8.6 | | | 7 | | |
| 1713 | 13.0 | 34 | 6.5 | 132 | 10.2 | | | 10 | | |
| 1719 | 9.0 | 40 | 6.7 | 104 | 17.3 | | | 3 | | |
| 1725 | 6.0 | 17 | 2.8 | 61 | 10.2 | | | 4 | | |
| 1727 | 2.0 | 13 | 6.5 | 36 | 18.0 | | | 1 | | |
| 1743 | 10.0 | 5 | 0.3 | 74 | 4.6 | | | 11 | | |
| 1744 | 1.0 | 12 | 12.0 | 56 | 58.0 | | | 0 | | |
| 18 9 | 25.0 | 4 | 0.2 | 62 | 2.5 | | | 11 | | |
| 1828 | 19.0 | 45 | 2.4 | 99 | 5.2 | | | 9 | | |

*Large headways indicate breaks in data.

APPENDIX 10 PROGRAM CONTRAC

Program CONTRAC contracts PAKPFL into half-hour intervals.

```
DIMENSION ITIME(1CC),INT(100),ICN(100),ICFF(1CC),
2 TCN(50),TCFF(50),TCHWY(50),HEDWAY(1CC),
2 RACN(50),RACFF(50).
DCUELE PRECISION FILECU, FILEIN
TYPE 5
5  FCRMAT('INPUT FILE NAME = ',$)
ACCEPT 6, FILEIN
6  FCRMAT(A10)
TYPE 7
7  FCRMAT('OLTPLT FILE NAME = ',$)
ACCEPT 6, FILEOU
OPEN(LUNIT=21,DEVICE='DSK',ACCESS='SEQIN',FILE=FILEIN)
OPEN(LUNIT=22,DEVICE='DSK',ACCESS='SEQOUT',FILE=FILECU)
DATA(INT(K),K=1,28)/700,730,800,830,900,930,1000,1030,
2 1100,1130,1200,1230,1300,1330,1400,1430,1500,1530,
2 1600,1630,1700,1730,1800,1830,1900,1930,2000,2030/
K=1
10 FCRMAT(///,2X,I4,4X,F5.1,5X,I3,14X,I3,19X)
11  DC 25 I=1,100
12  IF(I.EC.1)13,14
13  READ(21,1C)ITIME(I),HEDWAY(I),ICN(I),ICFF(I)
14  GO TO 15
14  READ(21,12,END=2C)ITIME(I),HEDWAY(I),ICN(I),ICFF(I)
15  FCRMAT(2X,I4,4X,F5.1,5X,I3,14X,I3,19X)
15  IF(ITIME(I).LE.INT(K))16,21
16  IF(HEDWAY(I).GT.30.0)25,18
18  TCHWY(K)=TCHWY(K)+HEDWAY(I)
18  TCN(K)=TCN(K)+ICN(I)
18  TCFF(K)=TCFF(K)+ICFF(I)
19  GO TO 25
20  M=1
21  IF(TCHWY(K).EQ.0)TCHWY(K)=1.0
21  RACN(K)=TCN(K)/TCHWY(K)
21  RACFF(K)=TCFF(K)/TCHWY(K)
21  WRITE(22,24)INT(K),RACN(K),RACFF(K)
24  FCRMAT(I4,1X,F6.2,1X,F6.2)
24  IF(M.EC.1)GC TC 30
24  K=K+1
24  GC TC 15
25  CONTINUE
30  END
```


APPENDIX 11 PROGRAM COMBIN

Program COMBIN combines all station data into an input matrix.

```
DIMENSION RACN(20,28),RACFF(20,28),INT(50)
DCUBLE PRECISICK FILEIN
OPEN(UNIT=23,DEVICE='DSK',ACCESS='SEQOUT',FILE='PASCUT.')
OPEN(UNIT=22,DEVICE='DSK',ACCESS='SEQOUT',FILE='PASSTIN.')
DATA(INT(K),K=1,26)/700,730,800,830,900,930,1000,1030,
2 1100,1130,1200,1230,1300,1230,1400,1430,1500,1530,
2 1600,1630,1700,1730,1800,1830,1900/
WRITE(5,1)
1  FCRMAT('NUMBER OF STATIONS= ', $)
ACCEPT 2, MS
2  FCRMAT(I2)
DC 50 I=1,MS
TYPE 6
6  FCRMAT('INPLT FILE = ', $)
ACCEPT 7, FILEIN
7  FORMAT(A10)
OPEN(UNIT=21,DEVICE='DSK',ACCESS='SEQIN',FILE=FILEIN)
DC 25 J=1,26
READ(21,10,END=12)RACN(I,J),RACFF(I,J)
10 FCRMAT(5X,F6.2,1X,F6.2)
GC TC 25
12  RAON(I,J)=0
RAOFF(I,J)=0
25  CCNTIME
CLOSE(UNIT=21)
50  CCNTINUE
DC 60 J=1,26
WRITE(22,52)INT(J),(RAON(I,J),I=1,MS)
52  FCRMAT(I4,1X,2E(F6.2))
60  CCNTINUE
DO 70 J=1,26
WRITE(23,52)INT(J),(RAOFF(I,J),I=1,MS)
70  CCNTINUE
END
```


APPENDIX 12 PROGRAM ESTREG

Program ESTREG estimates the missing values by regression.

```

DOUBLE PRECISION FILEIN,FILEOU
DIMENSION XBAR(35),SID(35),D(35),RY(35),ISAVE(35),B(35),
2 SB(35),T(35),W(35),RX(1500),R(1000),ANS(10),RATE(25,11),
2 PEATE(275),RES(275),OPATE(275),ERATE(275),Y(35,275),
2 Y2(35,275),TVAR(25,275),SVAE(11,275),P(35),X1(10000),
2 ,INT(25),TVAR1(25,275),SVAR1(11,275),B1(35),WK(35)
2 ,AL(275),BE(275),STRES(275)

1000  WRITE(5,1000)
      FORMAT('INPUT FILE = ',\$)
      ACCEPT 2000, FILEIN
2000  FORMAT(A10)
      WRITE(5,3000)
3000  FORMAT('OUTPUT FILE=' ,\$)
      ACCEPT 2000, FILEOU
      WRITE(5,4000)
4000  FORMAT('NUMBER OF STATIONS= ',\$)
      ACCEPI 5000, MS
5000  FORMAT(I2)
      WRITE(5,5000)
6000  FORMAT('NUMBER OF TIME PERIODS= ',\$)
      ACCEPT 5000, MT

      MK=MT+MS-1
      ML=MK-1
      MC=MT*MS

      OPEN(UNIT=21,DEVICE='DSK',ACCESS='SEQIN',FILE=FILEIN)
      OPEN(UNIT=22,DEVICE='DSK',ACCESS='SEQOUT',FILE=FILEOU)

      DO 5 I=1,MT
      READ(21,4) INT(I),(RATE(I,J),J=1,MS)
      4      FORMAT(I4,1X,11(F6.2))
      5      CONTINUE

      C      ESTABLISH INDEPENDENT VARIABLES Y
      M=0
      DO 12 I=1,MT
      DO 10 J=1,MS
      IF(RATE(I,J).EQ.0) GO TO 10
      10     M=M+1
      TVAR(I,M)=1
      SVAE(J,M)=1
      PRATE(M)= ALOG(RATE(I,J))
      12     CONTINUE
      CONTINUE

      DO 20 L=1,M
      Y(1,L)=PRATE(I)
      DO 13 I=1,MT-1
      Y(I+1,L)=TVAR(I,L)
      13     CONTINUE
      IF(TVAR(MT,L).NE.1) GO TO 15
      DO 14 I=1,MT-1
      Y(I+1,L)=-1
      14     CONTINUE
      DO 15 J=1,MS-1
      Y(MT+J,L)=SVAE(J,L)
      15     CONTINUE
      16     CONTINUE

```

PROGRAM ESTREG (CONT.)

```

IF (SVAR(MS,L).NE.1) GO TO 20
DO 17 J=1,MS-1
Y(MT+J,L)=-1
17  CONTINUE
20  CONTINUE

C      CONVERT Y TO DESIRED FORMAT OF REG. SUBROUTINE
K=0
DO 135 I=1,MK
DO 134 J=1,M
K=K+1
X1(K)=Y(I,J)
134  CONTINUE
135  CONTINUE

C      OBTAIN CORELATION MATRIX
CALL COPRE(M,MK,1,X1,XBAR,STD,FX,E,B1,D,T)

C      IDENTIFY INDEPENDENT VARIABLE VECTOR ISAVE
DO 165 L=1,ML
ISAVE(L)=L+1
165  CONTINUE

CALL OFDER(MK,E,1,ML,ISAVE,RX,RY)
CALL MINV(FX,ML,DET,WK,T)
CALL MULTR(M,ML,XBAR,STD,B1,FX,RY,ISAVE,B,SB,T,ANS)

WRITE(22,250)
250  FORMAT(18X,39HANALYSIS OF VARIANCE FOR THE REGRESSION//)
WRITE(22,252)
252  FORMAT(2X,19HSOURCE OF VARIATION,9X,2HDF,2X,13HSUM OF SQUARE
2,3X,11HMEAN SQUARE,6X,7HF-VALUE)
WRITE(22,260)ANS(5),ANS(4),ANS(6),ANS(10)
260  FORMAT(2X,26HATTRIBUTABLE TO REGRESSION,2X,F3.0,3X,
2F10.4,5X,F10.4,3X,F10.4)
WRITE(22,265)ANS(8),ANS(7),ANS(9)
265  FORMAT(2X,25HDEVIATION FROM REGRESSION,3X,F3.0,3X,F10.4,5X,
2F10.4,3X,F10.4)
WRITE(22,270)ANS(1)
270  FORMAT(//1X,10HINTERCEPT=F9.3)
ANS(2)=ANS(2)**2
WRITE(22,275)ANS(2)
275  FORMAT(1X,29HMULTIPLE CORE. COEFF. SQUARE=F6.5)
WRITE(22,280)ANS(3)
280  FORMAT(1X,27HSTANDARD ERROR OF ESTIMATE=F9.3//)
WRITE(22,290)
290  FORMAT(2X,8HVARIABLE,10X,12HREGF. COEFF.,10X,10HSTD.
2EFROR,10X,8HCOMPUTED)
WRITE(22,295)
295  FORMAT(43X,9HOF COEFF.,11X,7HT-VALUE//)
DO 310 J=1,ML
WRITE(22,300)ISAVE(J),B(J),SB(J),T(J)
300  FORMAT(6X,I2,14X,F10.4,11X,F9.4,10X,F9.4)
310  CONTINUE
DO 313 L=1,M
ALSO=0
BESO=0
ALSO1=0
BESO1=0
DO 311 K6=2,M
AL(I)=AL(I)+Y(K6,L)*B(K6-1)

```

PROGRAM ESTREG (CONT.)

```

ALSO=ALSO+B(K6-1)**2
ALSO1=ALSO1+B(K6-1)
CONTINUE
DO 312 K7=MT+1, MK
BE(L)=BE(L)+Y(K7,L)*B(K7-1)
BESQ=BESQ+B(K7-1)**2
BESQ1=BESQ1+B(K7-1)
312
CONTINUE
DS=DS+Y(1,L)*AL(L)*BE(L)
313
CONTINUE
ALSO=ALSO+ALSO1**2
BESQ=BESQ+BESQ1**2
DSTAT=(DS**2)/(ALSO*BESQ)
SSPE=ANS(7)-DSTAT
FSTAT=DSTAT*(ANS(8)-1)/SSPE
WRITE(22,314) FSTAT
314
FORMAT(///*THE INTERACTION TEST STAT. , FSTAT:,1X,F10.4)

C      OBTAIN ESTIMATES FOR MISSING VALUES AND RESIDUALS
KL=0
DO 320 I=1,MT
DO 315 J=1,MS
KL=KL+1
TVAE1(I,KL)=1
SVAE1(J,KL)=1
ORATE(KL)=RATE(I,J)
315
CONTINUE
CONTINUE
DO 330 L1=1,MC
DO 325 I=1,MT-1
Y2(I,L1)=TVAE1(I,L1)
325
CONTINUE
IF(TVAE1(MT,L1).NE.1) GO TO 327
DO 326 I=1,MT-1
Y2(I,L1)=-1
326
CONTINUE
DO 328 J=1,MS-1
Y2(MT-1+J,L1)=SVAE1(J,L1)
328
CONTINUE
IF(SVAE1(MS,L1).NE.1) GO TO 330
DO 329 J=1,MS-1
Y2(MT-1+J,L1)=-1
329
CONTINUE
330
CONTINUE

DO 340 L2=1,MC
T1=0
DO 335 K3=1,ML
T1=T1+B(K3)*Y2(K3,L2)
335
CONTINUE
ERATE(L2)=ANS(1)+T1
IF(ORATE(L2).NE.0) RES(L2)= ALOG(ORATE(L2))-ERATE(L2)
STRES(L2)=RES(L2)/SQRT(ANS(9))
ERATE(L2)=EXP(ERATE(L2))
340
CONTINUE

WRITE(22,350)
350
FORMAT(//,'ORIG. RATE',1X,'FITTED RATE',1X,'RESIDUAL',
2 1X, 'STAND. RES.')
DO 352 L2=1,MC
WRITE(22,351) ORATE(L2),ERATE(L2),RES(L2),STRES(L2)

```

PROGRAM ESTREG (CONT.)

```
351      FORMAT(2X,F6.2,4X,F6.2,4X,F6.2,5X,F6.2)
352      CONTINUE
      DO 353 L2=1,MC
      IF(ORATE(L2).NE.0) ERATE(L2)=ORATE(L2)
353      CONTINUE
      I=1
      L2=1
      WRITE(22,356)
356      FORMAT(///,'ESTIMATED UNLOADING RATE - ALL RIVERSIDE TRAINS',//,
      2 'TIME',2X,'KENMORE',1X,'AUDIT.',2X,'COPLEY',2X,'ARLING',
      2 2X,'BOYLST.',1X,'PK.ST.',2X,'GOV.CTR',1X,'HAYMKT',2X,
      2 'NOR.STA',1X,'SC.PK.',2X,'LECHMERE')
354      WRITE(22,355) INT(I),(ERATE(L2+J),J=0,MS-1)
      L2=L2+MS
      I=I+1
      IF(L2.LE.MC) GO TO 354
355      FORMAT(I4,2X,11(F6.2,2X))
400      END
      SUBROUTINE DATA
      RETURN
      END
```

APPENDIX 13
ANOVA RESULTS

RIVOFF.MTY; Model (3) analysis of variance for the regression (Transformed data)

| SOURCE OF VARIATION | DF | SUM OF SQUARE | MEAN SQUARE | F-VALUE |
|----------------------------|-----|---------------|-------------|---------|
| ATTRIBUTABLE TO REGRESSION | 31. | 146.3501 | 4.7210 | 10.0632 |
| DEVIATION FROM REGRESSION | 65. | 30.4937 | 0.4691 | |

INTERCEPT= 0.041
MULTIPLE CORR. COEFF. SQUARE=.82757
STANDARD ERROR OF ESTIMATE= 0.685

| VARIABLE | REGR. COEFF. | STD. ERROR, OF COEFF. | COMPUTED T-VALUE |
|----------|--------------|--------------------------|---------------------|
| 2 | 0.0421 | 0.7105 | 0.0593 |
| 3 | -0.5474 | 0.4024 | -1.3602 |
| 4 | 0.4067 | 0.2829 | 1.4374 |
| 5 | 0.6812 | 0.2829 | 2.4078 |
| 6 | 0.4350 | 0.3115 | 1.3966 |
| 7 | -0.2319 | 0.3465 | -0.6693 |
| 8 | 0.4156 | 0.3154 | 1.3177 |
| 9 | -0.1246 | 0.2897 | -0.4302 |
| 10 | -0.9837 | 0.3577 | -2.7498 |
| 11 | -0.3746 | 0.3577 | -1.0471 |
| 12 | -0.2753 | 0.4150 | -0.6633 |
| 13 | -0.6597 | 0.4010 | -1.6452 |
| 14 | -0.3688 | 0.7105 | -0.5191 |
| 15 | -0.3714 | 0.4881 | -0.7609 |
| 16 | 0.2183 | 0.3097 | 0.7049 |
| 17 | -0.1597 | 0.3097 | -0.5155 |
| 18 | -0.2602 | 0.3472 | -0.7493 |
| 19 | 0.3940 | 0.3472 | 1.1347 |
| 20 | 0.5742 | 0.3456 | 1.6613 |
| 21 | 0.7678 | 0.3456 | 2.2213 |
| 22 | 0.7146 | 0.3113 | 2.2955 |
| 23 | 0.4602 | 0.3456 | 1.3313 |
| 24 | 0.9076 | 0.3113 | 2.9152 |
| 25 | 0.2987 | 0.3965 | 0.7533 |
| 26 | 0.8251 | 0.1534 | 5.3781 |
| 27 | 0.0963 | 0.3139 | 0.3067 |
| 28 | 1.4366 | 0.2711 | 5.2982 |
| 29 | 0.9529 | 0.2303 | 4.1369 |
| 30 | -0.7833 | 0.1937 | -4.0432 |
| 31 | 0.8289 | 0.1720 | 4.8184 |
| 32 | -0.7414 | 0.2025 | -3.6609 |

THE INTERACTION TEST STAT. , FSTAT: 10.0026

ANOVA RESULTS (CONT.)

NORON.MTY; Model (3) analysis of variance for the regression (Transformed data)

| SOURCE OF VARIATION | DF | SUM OF SQUARE | MEAN SQUARE | F-VALUE |
|----------------------------|-----|---------------|-------------|---------|
| ATTRIBUTABLE TO REGRESSION | 30. | 111.1235 | 3.7041 | 5.8990 |
| DEVIATION FROM REGRESSION | 66. | 41.4427 | 0.6279 | |

INTERCEPT = -0.375
 MULTIPLE CORR. COEFF. SQUARE=.72836
 STANDARD ERROR OF ESTIMATE = 0.792

| VARIABLE | REGR. COEFF. | STD. ERROR, OF COEFF. | COMPUTED T-VALUE |
|----------|--------------|--------------------------|---------------------|
| 2 | -1.7435 | 0.8023 | -2.1733 |
| 3 | -1.3899 | 0.8023 | -1.7325 |
| 4 | 0.3695 | 0.4577 | 0.8074 |
| 5 | 0.2950 | 0.3573 | 0.8256 |
| 6 | 0.4035 | 0.4034 | 1.0003 |
| 7 | -0.2205 | 0.3640 | -0.6057 |
| 8 | -0.4674 | 0.3681 | -1.2699 |
| 9 | -0.3418 | 0.3152 | -1.0843 |
| 10 | 0.0007 | 0.3092 | 0.0023 |
| 11 | -0.3389 | 0.3331 | -1.0175 |
| 12 | -0.7660 | 0.3984 | -1.9228 |
| 13 | -0.4118 | 0.4562 | -0.9026 |
| 14 | -0.4933 | 0.7843 | -0.6289 |
| 15 | -0.0676 | 0.4630 | -0.1460 |
| 16 | -0.0327 | 0.4630 | -0.0707 |
| 17 | -0.0525 | 0.4630 | -0.1134 |
| 18 | 0.4997 | 0.8023 | 0.6229 |
| 19 | 1.3250 | 0.7955 | 1.6655 |
| 20 | 0.6679 | 0.4604 | 1.4508 |
| 21 | 0.8779 | 0.3381 | 2.5966 |
| 22 | 0.9597 | 0.3152 | 3.0446 |
| 23 | 1.1004 | 0.3152 | 3.4911 |
| 24 | -0.0027 | 0.3387 | -0.0081 |
| 25 | 0.9726 | 0.1869 | 5.2039 |
| 26 | 0.6689 | 0.2695 | 2.4819 |
| 27 | 1.0098 | 0.2749 | 3.6734 |
| 28 | 0.4497 | 0.2338 | 1.9238 |
| 29 | -1.0271 | 0.2553 | -4.0236 |
| 30 | 0.6594 | 0.2184 | 3.0192 |
| 31 | -0.9677 | 0.1979 | -4.8885 |

THE INTERACTION TEST STAT. , FSTAT: 2.3866

ANOVA RESULTS (CONT.)

NOROFF.MTY; Model (3) analysis of variance for the regression (Transformed data)

| SOURCE OF VARIATION | DF | SUM OF SQUARE | MEAN SQUARE | F-VALUE |
|----------------------------|-----|---------------|-------------|---------|
| ATTRIBUTABLE TO REGRESSION | 31, | 117,3748 | 3,7863 | 9,8920 |
| DEVIATION FROM REGRESSION | 76, | 29,0901 | 0,3828 | |

INTERCEPT = 0,505
 MULTIPLE CORR. COEFF. SQUARE = .80139
 STANDARD ERROR OF ESTIMATE = 0,619

| VARIABLE | REGR. COEFF. | STD. ERROR, OF COEFF. | COMPUTED T-VALUE |
|----------|--------------|--------------------------|---------------------|
| 2 | -0,9219 | 0,6248 | -1,4756 |
| 3 | -0,2182 | 0,6248 | -0,3493 |
| 4 | 1,0731 | 0,3116 | 3,4433 |
| 5 | 0,4788 | 0,2555 | 1,8745 |
| 6 | 0,6644 | 0,2818 | 2,3573 |
| 7 | -0,1813 | 0,2578 | -0,7034 |
| 8 | 0,0581 | 0,2611 | 0,2226 |
| 9 | -0,1435 | 0,2432 | -0,5901 |
| 10 | -0,1912 | 0,2251 | -0,8492 |
| 11 | -0,5318 | 0,2843 | -1,8705 |
| 12 | -0,2032 | 0,3106 | -0,6543 |
| 13 | 0,1756 | 0,3560 | 0,4931 |
| 14 | 0,1775 | 0,4449 | 0,3990 |
| 15 | -0,4322 | 0,3134 | -1,3789 |
| 16 | 0,3830 | 0,3134 | 1,2219 |
| 17 | 0,1668 | 0,3134 | 0,5322 |
| 18 | 0,1217 | 0,4408 | 0,2760 |
| 19 | 0,2178 | 0,6198 | 0,3514 |
| 20 | -0,1526 | 0,3583 | -0,4260 |
| 21 | 0,0275 | 0,2611 | 0,1053 |
| 22 | -0,0830 | 0,2432 | -0,3412 |
| 23 | 0,0772 | 0,2432 | 0,3172 |
| 24 | -0,1637 | 0,2432 | -0,6732 |
| 25 | -1,2278 | 0,1476 | -8,3207 |
| 26 | -0,3277 | 0,2146 | -1,5274 |
| 27 | -0,3381 | 0,2045 | -1,6531 |
| 28 | -0,1479 | 0,1837 | -0,9050 |
| 29 | -0,9634 | 0,2033 | -4,7392 |
| 30 | 1,6122 | 0,1704 | 9,4595 |
| 31 | 1,1294 | 0,1549 | 7,2908 |
| 32 | 0,2395 | 0,1785 | 1,3416 |

THE INTERACTION TEST STAT. , FSTAT: 16,3779

HE 18.5 A37
UMIA-
Kunk, Petty
- Passenger f
1978. Rive
-

Form DOT F 1720
FORMERLY FORM DOT

00010000

**U.S. DEPARTMENT OF TRANSPORTATION
RESEARCH AND SPECIAL PROGRAMS ADMINISTRATION
TRANSPORTATION SYSTEMS CENTER**

CAMBRIDGE, MA. 02142

OFFICIAL BUSINESS

PENALTY FOR PRIVATE USE, \$200

POSTAGE AND FEES PAID
U. S. DEPARTMENT OF TRANSPORTATION
613

